

# TECHNICAL DATA

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# LIST OF PROPERTY SYMBOLS COMPLYING WITH ISO13399

Alphabetical

Source: ISO13399 standard

URL : <https://www.iso.org/search/x/query/13399>

ISO13399 Property Symbols	Content
<b>ADJLX</b>	Adjustment limit maximum
<b>ADJRG</b>	Adjustment range
<b>ALF</b>	Clearance angle radial
<b>ALP</b>	Clearance angle axial
<b>AN</b>	Clearance angle major
<b>ANN</b>	Clearance angle minor
<b>APMX</b>	Depth of cut maximum
<b>AS</b>	Clearance angle wiper edge
<b>ASP</b>	Adjusting screw protrusion
<b>AZ</b>	Plunge depth maximum
<b>B</b>	Shank width
<b>BBD</b>	Balanced by design
<b>BCH</b>	Corner chamfer length
<b>BD</b>	Body diameter
<b>BDX</b>	Body diameter maximum
<b>BHCC</b>	Bolt hole circle count
<b>BHTA</b>	Body half taper angle
<b>BMC</b>	Body material code
<b>BS</b>	Wiper edge length
<b>BSR</b>	Wiper edge radius
<b>CASC</b>	Cartridge size code
<b>CB</b>	Chip breaker face count
<b>CBDP</b>	Connection bore depth
<b>CBMD</b>	Chip breaker manufacturers designation
<b>CBP</b>	Chip breaker property
<b>CCMS</b>	Connection code machine side
<b>CCWS</b>	Connection code workpiece side
<b>CCP</b>	Chamfer corner property
<b>CDI</b>	Insert cutting diameter
<b>CDX</b>	Cutting depth maximum
<b>CEATC</b>	Tool cutting edge angle type code
<b>CECC</b>	Cutting edge condition code
<b>CEDC</b>	Cutting edge count
<b>CF</b>	Spot chamfer
<b>CHW</b>	Corner chamfer width
<b>CICT</b>	Cutting item count
<b>CNC</b>	Corner count
<b>CND</b>	Coolant entry diameter
<b>CNSC</b>	Coolant entry style code
<b>CNT</b>	Coolant entry thread size
<b>CP</b>	Coolant pressure
<b>CRE</b>	Spot radius
<b>CRKS</b>	Connection retention knob thread size
<b>CSP</b>	Coolant supply property
<b>CTP</b>	Coating property
<b>CTX</b>	Cutting point translation X-direction
<b>CTY</b>	Cutting point translation Y-direction
<b>CUTDIA</b>	Work piece parting diameter maximum
<b>CUB</b>	Connection unit basis
<b>CW</b>	Cutting width
<b>CWX</b>	Cutting width maximum
<b>CXD</b>	Coolant exit diameter

ISO13399 Property Symbols	Content
<b>CXSC</b>	Coolant exit style code
<b>CZC</b>	Connection size code
<b>D1</b>	Fixing hole diameter
<b>DAH</b>	Diameter access hole
<b>DAXN</b>	Axial groove outside diameter minimum
<b>DAXX</b>	Axial groove outside diameter maximum
<b>DBC</b>	Diameter bolt circle
<b>DC</b>	Cutting diameter
<b>DCB</b>	Connection bore diameter
<b>DCBN</b>	Connection bore diameter minimum
<b>DCBX</b>	Connection bore diameter maximum
<b>DCC</b>	Design configuration style code
<b>DCCB</b>	Counterbore diameter connection bore
<b>DCIN</b>	Cutting diameter internal
<b>DCINN</b>	Cutting diameter internal minimum
<b>DCINX</b>	Cutting diameter internal maximum
<b>DCN</b>	Cutting diameter minimum
<b>DCON</b>	Connection diameter
<b>DCONMS</b>	Connection diameter machine side
<b>DCONWS</b>	Connection diameter workpiece side
<b>DCSC</b>	Cutting diameter size code
<b>DCSFMS</b>	Contact surface diameter machine side
<b>DCX</b>	Cutting diameter maximum
<b>DF</b>	Flange diameter
<b>DHUB</b>	Hub diameter
<b>DMIN</b>	Minimum bore diameter
<b>DMM</b>	Shank diameter
<b>DN</b>	Neck diameter
<b>DRVA</b>	Drive angle
<b>EPSR</b>	Insert included angle
<b>FHA</b>	Flute helix angle
<b>FHCSA</b>	Fixing hole countersunk angle
<b>FHCSD</b>	Fixing hole countersunk diameter
<b>FLGT</b>	Flange thickness
<b>FMT</b>	Form type
<b>FXHLP</b>	Fixing hole property
<b>GAMF</b>	Rake angle radial
<b>GAMN</b>	Rake angle normal
<b>GAMO</b>	Rake angle orthogonal
<b>GAMP</b>	Rake angle axial
<b>GAN</b>	Insert rake angle
<b>H</b>	Shank height
<b>HA</b>	Thread height theoretical
<b>HAND</b>	Hand
<b>HBH</b>	Head bottom offset height
<b>HBKL</b>	Head back offset length
<b>HBKW</b>	Head back offset width
<b>HBL</b>	Head bottom offset length
<b>HC</b>	Thread height actual
<b>HF</b>	Functional height
<b>HHUB</b>	Hub height
<b>HTB</b>	Body height
<b>IC</b>	Inscribed circle diameter
<b>IFS</b>	Insert mounting style code
<b>IIC</b>	Insert interface code
<b>INSL</b>	Insert length
<b>KAPR</b>	Tool cutting edge angle
<b>KCH</b>	Corner chamfer angle

# LIST OF PROPERTY SYMBOLS COMPLYING WITH ISO13399

ISO13399 Property Symbols	Content
<b>KRINS</b>	Cutting edge angle major
<b>KWL</b>	Keyway length
<b>KWW</b>	Keyway width
<b>KYP</b>	Keyway property
<b>L</b>	Cutting edge length
<b>LAMS</b>	Inclination angle
<b>LB</b>	Body length
<b>LBB</b>	Chip breaker width
<b>LBX</b>	Body length maximum
<b>LCCB</b>	Counterbore depth connection bore
<b>LCF</b>	Length chip flute
<b>LDRED</b>	Reduced body diameter length
<b>LE</b>	Cutting edge effective length
<b>LF</b>	Functional length
<b>LFA</b>	A dimension on If
<b>LH</b>	Head length
<b>LPR</b>	Protruding length
<b>LS</b>	Shank length
<b>LSC</b>	Clamping length
<b>LSCN</b>	Clamping length minimum
<b>LSCX</b>	Clamping length maximum
<b>LTA</b>	LTA length (length from MCS to CRP)
<b>LU</b>	Usable length
<b>LUX</b>	Usable length maximum
<b>M</b>	M-dimension
<b>M2</b>	Distance between the nominal inscribed circle and the corner of an insert that has the secondary included angle
<b>MHA</b>	Mounting hole angle
<b>MHD</b>	Mounting hole distance
<b>MHH</b>	Mounting hole height
<b>MIID</b>	Master insert identification
<b>MTP</b>	Clamping type code
<b>NCE</b>	Cutting end count
<b>NOF</b>	Flute count
<b>NOI</b>	Insert index count
<b>NT</b>	Tooth count
<b>OAH</b>	Overall height
<b>OAL</b>	Overall length
<b>OAW</b>	Overall width
<b>PDPT</b>	Profile depth insert
<b>PDX</b>	Profile distance ex
<b>PDY</b>	Profile distance ey
<b>PFS</b>	Profile style code
<b>PL</b>	Point length
<b>PNA</b>	Profile included angle
<b>PSIR</b>	Tool lead angle
<b>PSIRL</b>	Cutting edge angle major left hand
<b>PSIRR</b>	Cutting edge angle major right hand
<b>RAL</b>	Relief angle left hand
<b>RAR</b>	Relief angle right hand
<b>RCP</b>	Rounded corner property
<b>RE</b>	Corner radius
<b>REL</b>	Corner radius left hand
<b>RER</b>	Corner radius right hand
<b>RMPX</b>	Ramping angle maximum
<b>RPMX</b>	Rotational speed maximum
<b>S</b>	Insert thickness
<b>S1</b>	Insert thickness total

ISO13399 Property Symbols	Content
<b>SC</b>	Insert shape code
<b>SDL</b>	Step diameter length
<b>SIG</b>	Point angle
<b>SSC</b>	Insert seat size code
<b>SX</b>	Shank cross section shape code
<b>TC</b>	Tolerance class insert
<b>TCE</b>	Tipped cutting edge code
<b>TCTR</b>	Thread tolerance class
<b>TD</b>	Thread diameter
<b>THFT</b>	Thread form type
<b>THL</b>	Threading length
<b>THLGTH</b>	Thread length
<b>THSC</b>	Tool holder shape code
<b>THUB</b>	Hub thickness
<b>TP</b>	Thread pitch
<b>TPI</b>	Threads per inch
<b>TPIN</b>	Threads per inch minimum
<b>TPIX</b>	Threads per inch maximum
<b>TPN</b>	Thread pitch minimum
<b>TPT</b>	Thread profile type
<b>TPX</b>	Thread pitch maximum
<b>TQ</b>	Torque
<b>TSYC</b>	Tool style code
<b>TTA</b>	Thread type
<b>ULDR</b>	Usable length diameter ratio
<b>UST</b>	Unit system
<b>W1</b>	Insert width
<b>WEP</b>	Wiper edge property
<b>WF</b>	Functional width
<b>WF2</b>	Distance between the cutting reference point and the front seating surface of a turning tool
<b>WFS</b>	Functional width secondary
<b>WT</b>	Weight of item
<b>ZEFF</b>	Face effective cutting edge count
<b>ZEFP</b>	Peripheral effective cutting edge count
<b>ZNC</b>	Cutting edge centre count
<b>ZNF</b>	Face mounted insert count
<b>ZNP</b>	Peripheral mounted insert count

## LIST OF REFERENCE SYMBOLS COMPLYING WITH ISO13399

ISO13399 Reference Symbols	Content
<b>CIP</b>	Coordinate system in process
<b>CRP</b>	Cutting reference point
<b>CSW</b>	Coordinate system workpiece side
<b>MCS</b>	Mounting coordinate system
<b>PCS</b>	Primary coordinate system

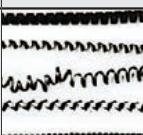
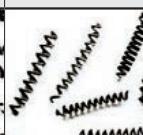
# TROUBLE SHOOTING FOR TURNING

		Solution	Insert Grade Selection		Cutting Conditions			Style and Design of the Tool			Machine, Installation of Tool		
Trouble	Factors		Select a harder grade	Select a tougher grade	Cutting speed	Feed	Depth of cut	Coolant	Rake	Corner radius	Lead angle	Honing strengthens the cutting edge	
Deterioration of Tool Life	Insert wear quickly generated	Improper tool grade	●										
		Improper cutting edge geometry											
		Improper cutting speed			↖●	↗●		Wet	●	↗●	↗●	↗●	
	Chipping or fracturing of cutting edge	Improper tool grade		●									
		Improper cutting conditions				↖●	↗●						
		Lack of cutting edge strength.					↖●			↗●	↗●		
		Thermal crack occurs		●	↖●	↖●	↖●	Dry					
		Build-up edge occurs		●	↗●	↗●	●	Wet	●				
Out of Tolerance	Dimensions are not constant	Poor insert accuracy											
		Large cutting resistance and cutting edge flank											
	Necessary to adjust often because of over-size	Improper tool grade	●										
		Improper cutting conditions			↖●	↗●							
	Deterioration of Surface Finish	Welding occurs			↗●			Wet					
		Improper cutting edge geometry											
		Chattering			↖●	↖●	↖●			↗●			
Generation of Heat	Workpiece over heating can cause poor accuracy and short life of insert	Improper cutting conditions			↖●	↖●	↖●						
		Improper cutting edge geometry							●	↗●			

Solution		Insert Grade Selection				Cutting Conditions			Style and Design of the Tool				Machine, Installation of Tool		
		Select a harder grade	Select a tougher grade	Select a grade with better thermal shock resistance	Select a grade with better adhesion resistance	Cutting speed	Feed	Depth of cut	Coolant	Rake	Corner radius	Lead angle	Honing strengthens the cutting edge		
Trouble	Factors	Up ↗	Down ↘	Up ↗	Down ↘	Up ↗	Down ↘	Up ↗	Down ↘	Up ↗	Down ↘	Up ↗	Down ↘	Class of insert	Improve tool holder rigidity
Burr, Chipping etc.	Burrs (Steel, Aluminium)	Notch wear	●												
		Improper cutting conditions				↖ ●	↗ ●		● Wet						
		Improper cutting edge geometry								● ↗	● ↗	● ↗	● ↗		
Workpiece chipping (Cast iron)	Workpiece chipping (Cast iron)	Improper cutting conditions				↖ ●	↖ ●								
		Improper cutting edge geometry								● ↗	● ↗	● ↗	● ↗		
		Vibration occurs												●	●
Poor Chip Dispersal	Burrs (Mild steel)	Improper tool grade		●											
		Improper cutting conditions			↗ ●				● Wet						
		Improper cutting edge geometry								● ↗	● ↗	● ↗	↖ ●		
		Vibration occurs												●	●
Long chips	Long chips	Improper cutting conditions			↖ ●	↗ ●	↗ ●		● Wet						
		Large chip control range								●					
		Improper cutting edge geometry								● ↗	● ↗				
Chips are short and scattered	Chips are short and scattered	Improper cutting conditions			↖ ●	↖ ●	↖ ●		● Dry						
		Small chip control range								●					
		Improper cutting edge geometry								↖ ●	↖ ●				

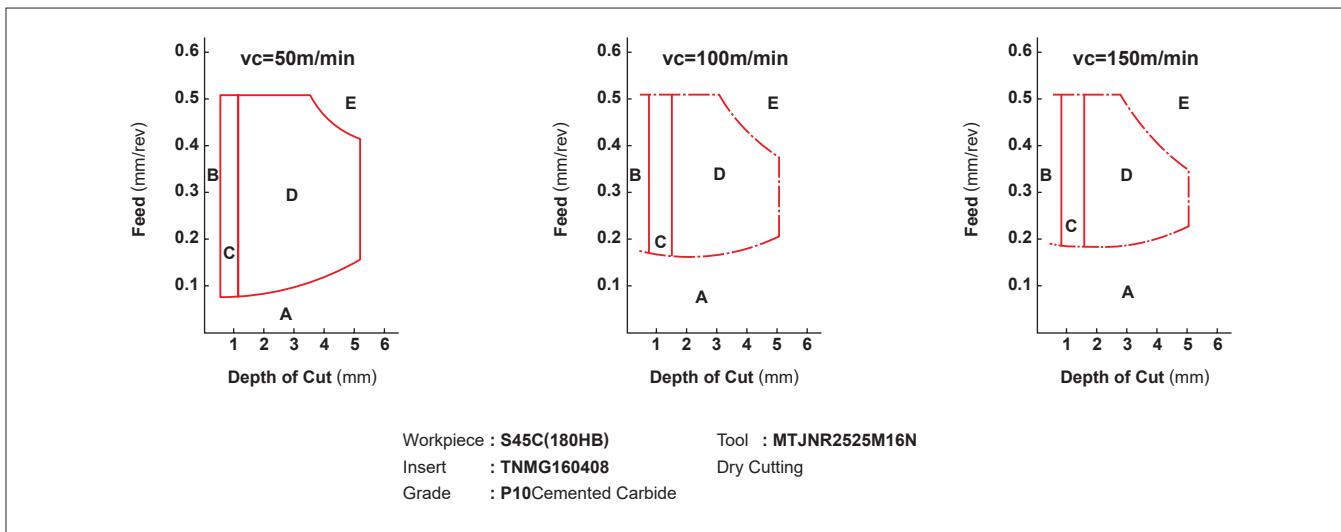
# CHIP CONTROL FOR TURNING

## CHIP BREAKING CONDITIONS IN STEEL TURNING

Type	A Type	B Type	C Type	D Type	E Type
Small Depth of Cut $d < 7\text{mm}$					
Small Depth of Cut $d=7\text{--}15\text{mm}$					
Curl Length I	Curless	$I \geq 50\text{mm}$	$I \leq 50\text{mm}$ 1-5 Curl	$\approx 1$ Curl	Less Than 1 Curl Half a Curl
Note	<ul style="list-style-type: none"> <li>● Irregular continuous shape</li> <li>● Tangle around tool and workpiece</li> </ul>	<ul style="list-style-type: none"> <li>● Regular continuous shape</li> <li>● Long chips</li> </ul>	Good	Good	<ul style="list-style-type: none"> <li>● Chip scattering</li> <li>● Chattering</li> <li>● Poor finished surface</li> <li>● Maximum</li> </ul>

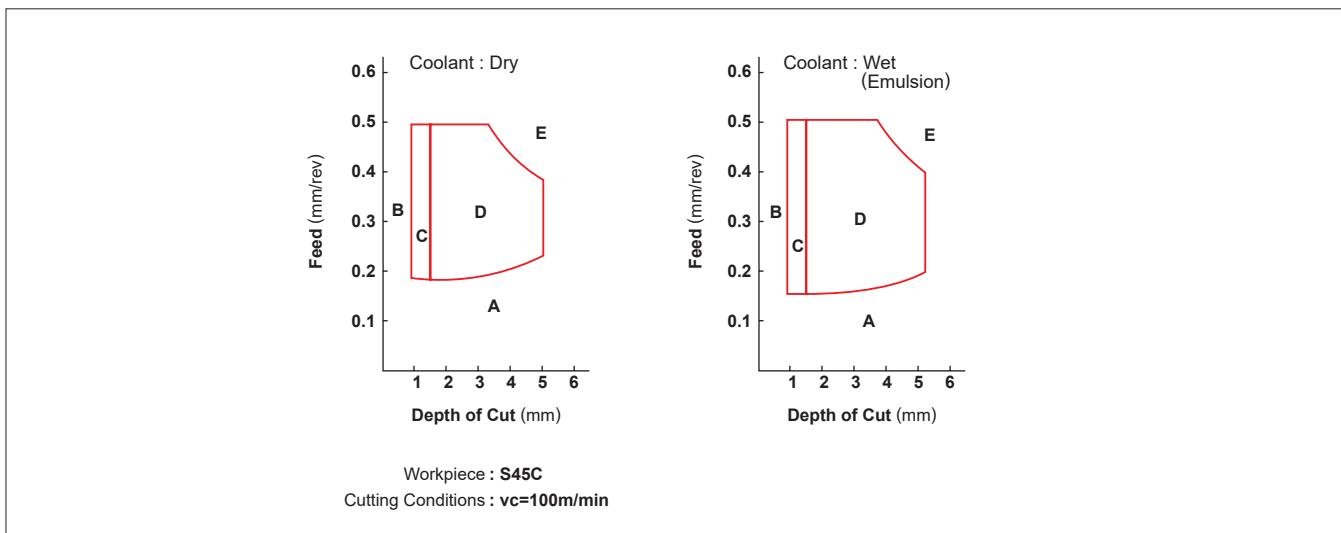
## Cutting speed and chip control range of chip breaker

In general, when cutting speed increases, the chip control range tends to become narrower.



## Effects of coolant on the chip control range of a chip breaker

If the cutting speed is the same, the range of chip control differs according to whether coolant is used or not.



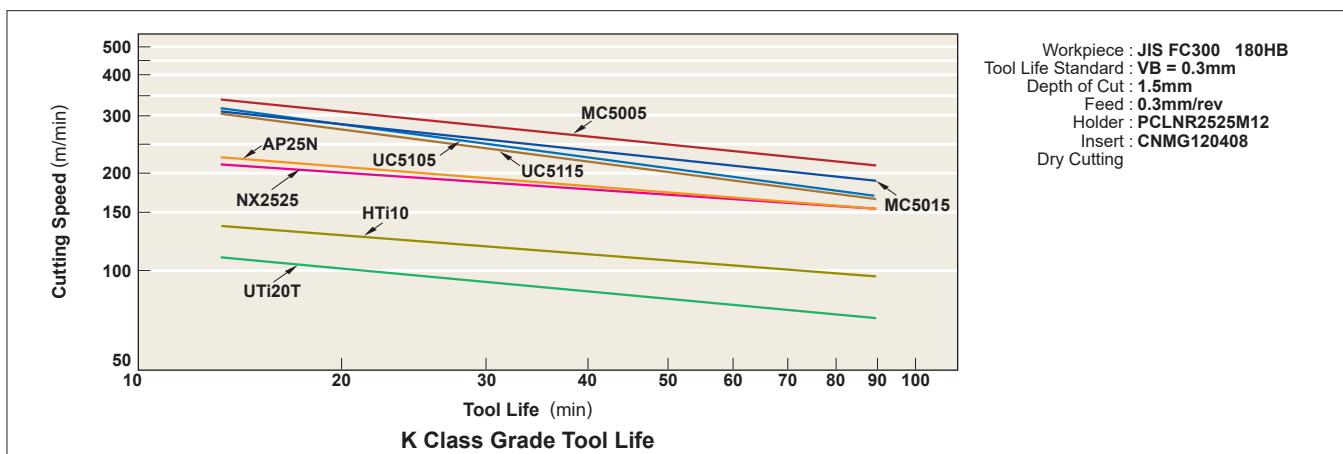
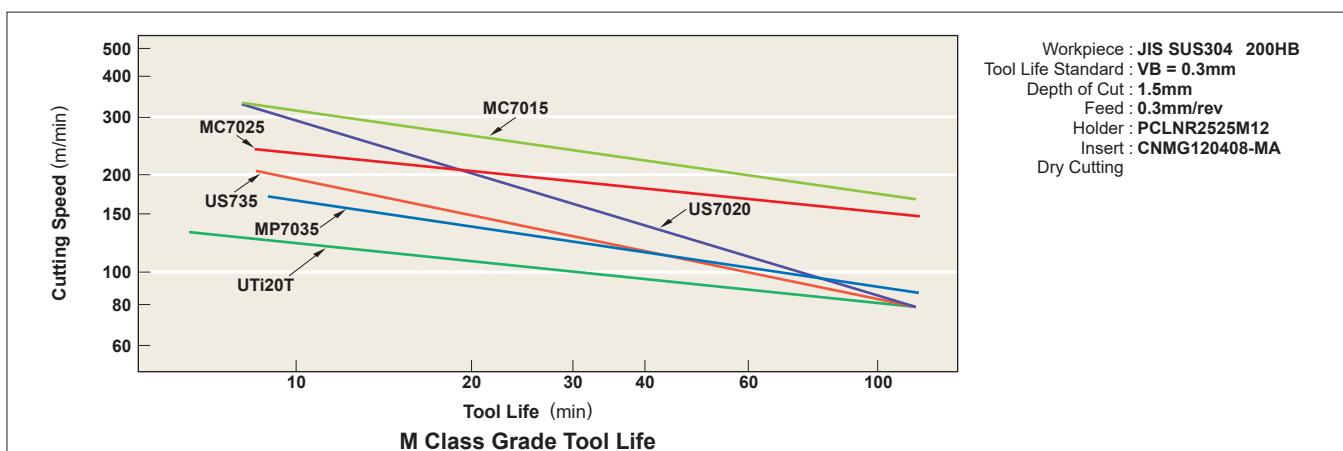
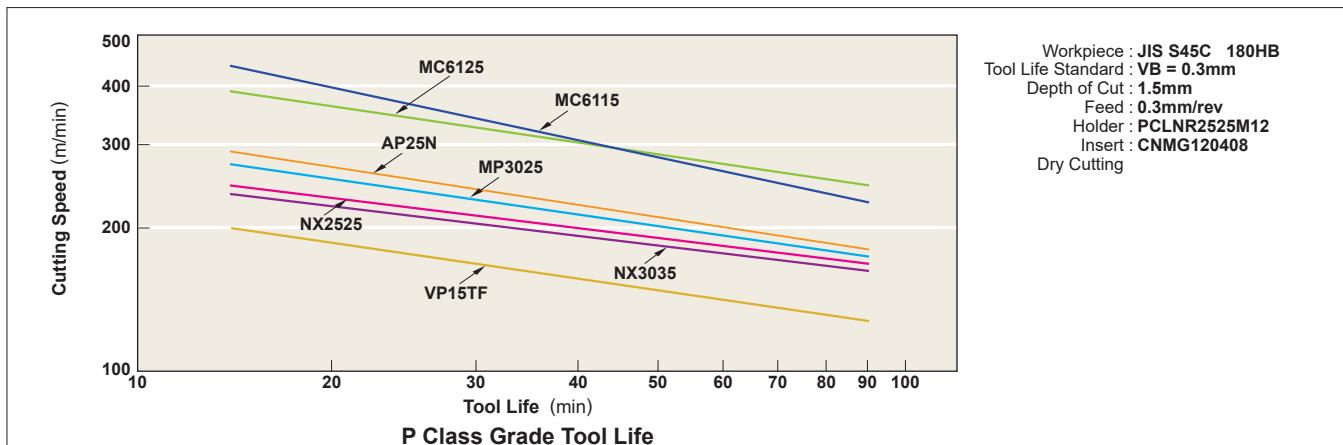
# EFFECTS OF CUTTING CONDITIONS FOR TURNING

## ■EFFECTS OF CUTTING CONDITIONS

Ideal conditions for cutting are short cutting time, long tool life, and high cutting accuracy. In order to obtain these conditions, selection of efficient cutting conditions and tools, based on workpiece material, hardness, shape and machine capability is necessary.

## ■CUTTING SPEED

Cutting speed effects tool life greatly. Increasing cutting speed increases cutting temperature and results in shortening tool life. Cutting speed varies depending on the type and hardness of the workpiece material. Selecting a tool grade suitable for the cutting speed is necessary.



### ●Effects of Cutting Speed

1. Increasing cutting speed by 20% decreases tool life by 50%. Increasing cutting speed by 50% decreases tool life by 80%.
2. Cutting at low cutting speed (20–40m/min) tends to cause chattering. Thus, tool life is shortened.

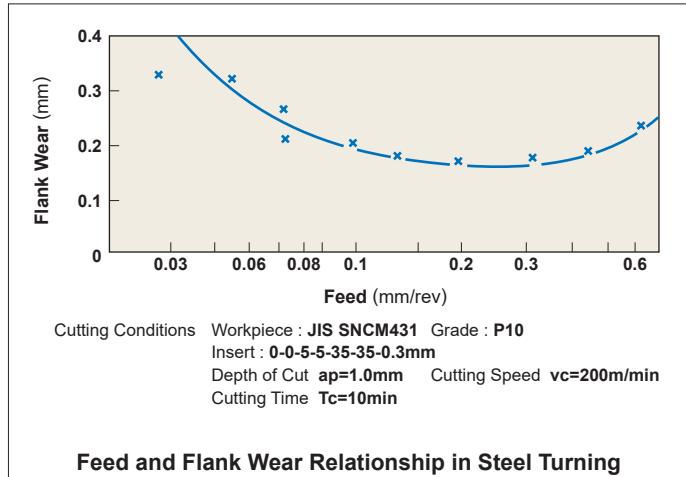
# EFFECTS OF CUTTING CONDITIONS FOR TURNING

## ■ FEED

When cutting with a general type holder, feed is the distance a holder moves per workpiece revolution. When milling, feed is the distance a machine table moves per cutter revolution divided by the number of inserts. Thus, it is indicated as feed per tooth. Feed rate relates to finished surface roughness.

### ● Effects of Feed

- Decreasing feed rate results in flank wear and shortens tool life.
- Increasing feed rate increases cutting temperature and flank wear. However, effects on the tool life is minimal compared to cutting speed.
- Increasing feed rate improves machining efficiency.

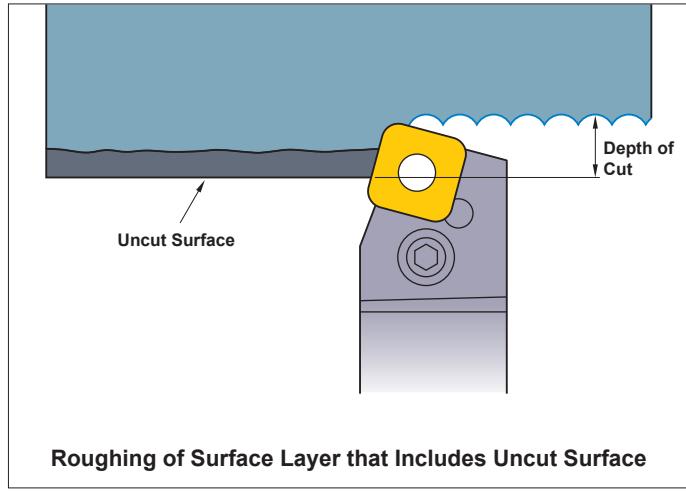
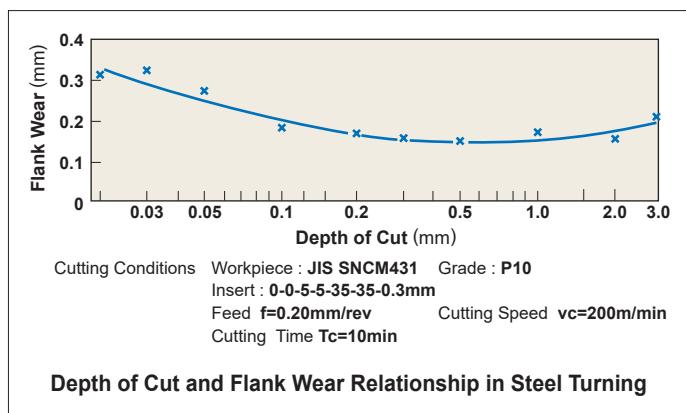


## ■ DEPTH OF CUT

Depth of cut is determined according to the required stock removal, shape of workpiece, power and rigidity of the machine and tool rigidity.

### ● Effects of Depth of Cut

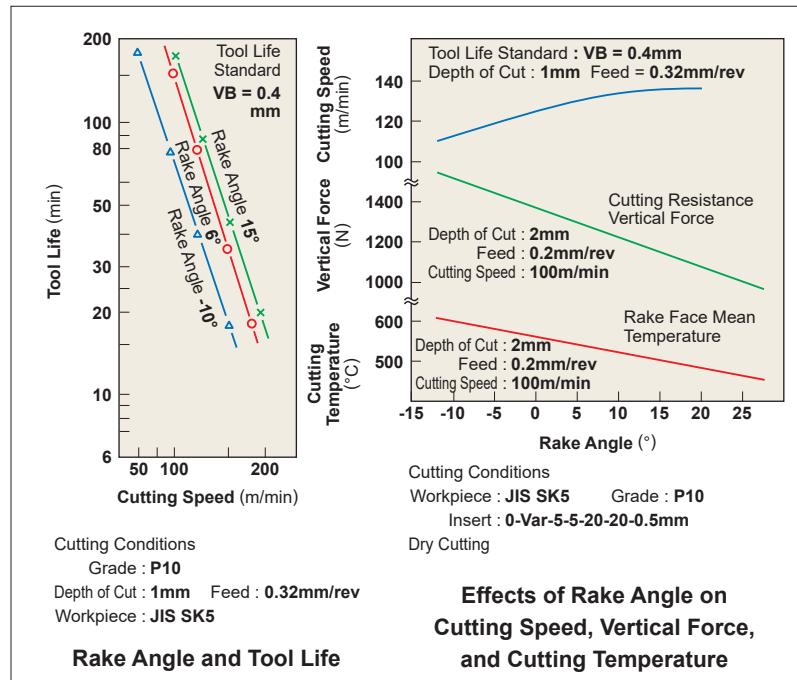
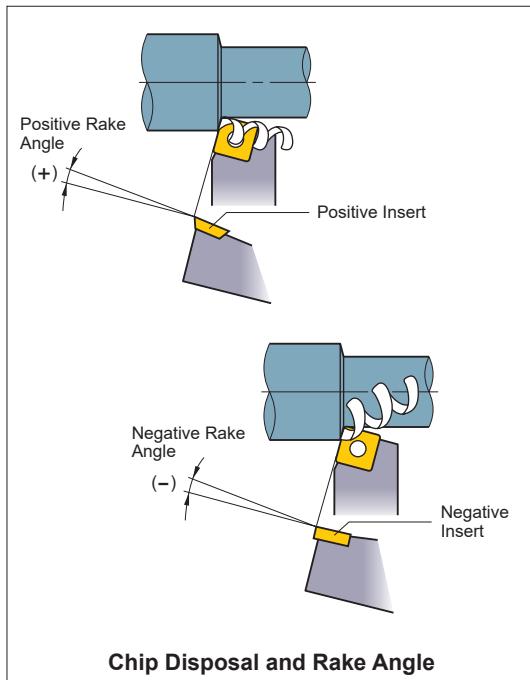
- Changing depth of cut doesn't effect tool life greatly.
- Small depths of cut result in friction when cutting the hardened layer of a workpiece. Thus tool life is shortened.
- When cutting uncut surfaces or cast iron surfaces, the depth of cut needs to be increased as much as the machine power allows in order to avoid cutting impure hard layers with the tip of cutting edge to prevent chipping and abnormal wear.



# FUNCTION OF TOOL FEATURES FOR TURNING

## ■RAKE ANGLE

Rake angle is cutting edge angle that has a large effect on cutting resistance, chip disposal, cutting temperature and tool life.



### ●Effects of Rake Angle

- Increasing rake angle in the positive (+) direction improves sharpness.
- Increasing rake angle by 1° in the positive (+) direction decreases cutting power by about 1%.
- Increasing rake angle in the positive (+) direction lowers cutting edge strength and in the negative (-) direction increases cutting resistance.

### When to Increase Rake Angle in the Negative (-) Direction

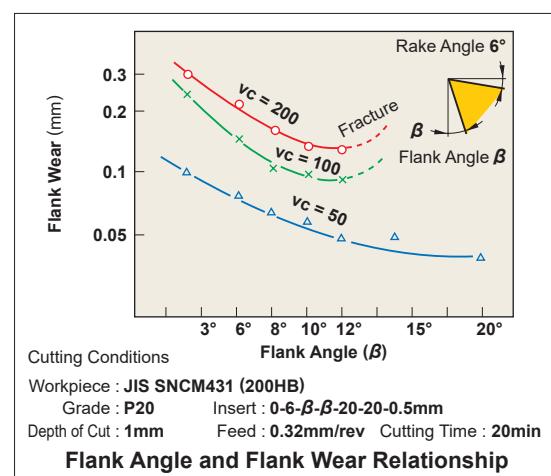
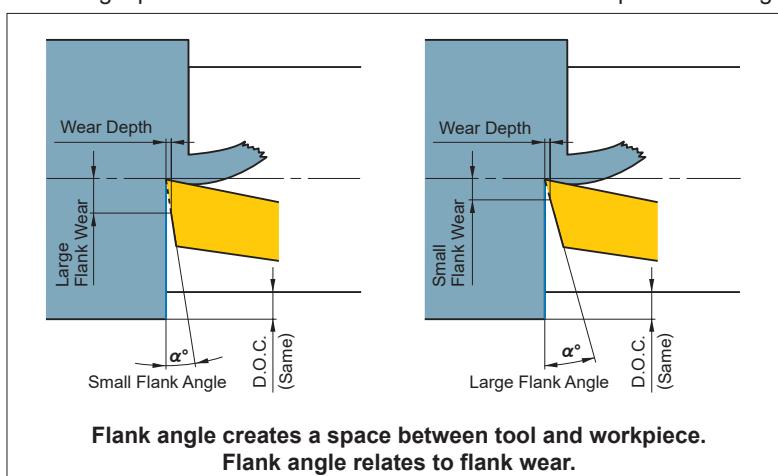
- Hard workpieces.
- When the cutting edge strength is required such as for uncut surfaces and interrupted cutting.

### When to Increase Rake Angle in the Positive (+) Direction

- Soft workpieces.
- Workpiece is easily machined.
- When the workpiece or the machine have poor rigidity.

## ■FLANK ANGLE

Flank angle prevents friction between flank face and workpiece resulting in smooth feed.



### ●Effects of Rake Angle

- Increasing flank angle decreases flank wear occurrence.
- Increasing flank angle lowers cutting edge strength.

### When to Decrease Flank Angle

- Hard workpieces.
- When cutting edge strength is required.

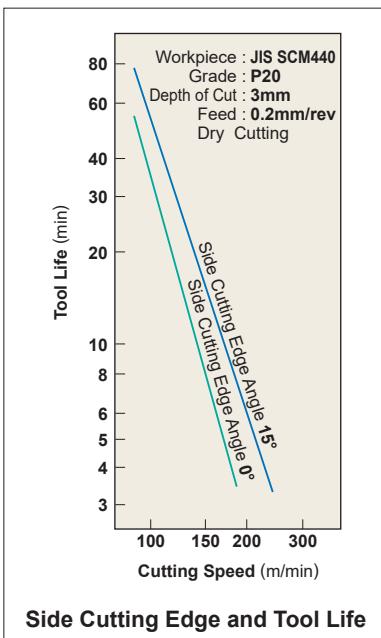
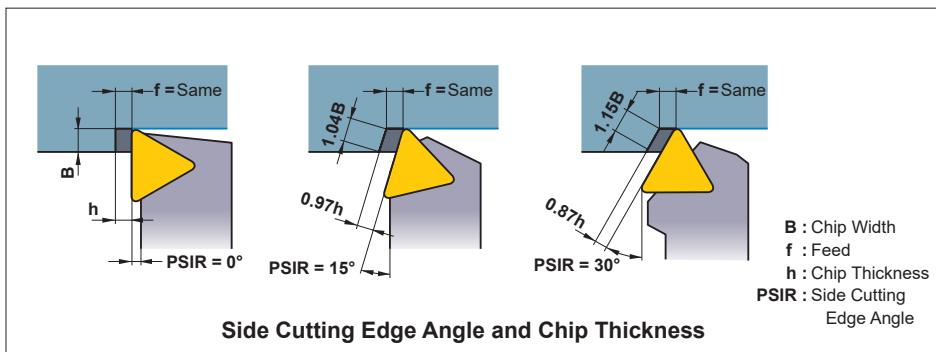
### When to Increase Flank Angle

- Soft workpieces.
- Workpieces suffer from work hardening easily.

# FUNCTION OF TOOL FEATURES FOR TURNING

## SIDE CUTTING EDGE ANGLE (LEAD ANGLE)

The side cutting edge angle reduces impact load and effects the amount of feed force, back force and chip thickness.

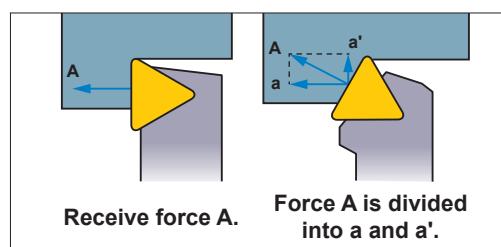


### Effects of Side Cutting Edge Angle (Lead Angle)

- At the same feed rate, increasing the side cutting edge angle increases the chip contact length and decreases chip thickness. As a result, the cutting force is dispersed on a longer cutting edge and tool life is prolonged. (Refer to the chart.)
- Increasing the side cutting edge angle increases force  $a'$ . Thus, thin, long workpieces suffer from bending in some cases.
- Increasing the side cutting edge angle decreases chip control.
- Increasing the side cutting edge angle decreases the chip thickness and increases chip width. Thus, breaking chips is difficult.

When to Decrease Lead Angle
<ul style="list-style-type: none"> <li>○ Finishing with small depth of cut.</li> <li>○ Thin, long workpieces.</li> <li>○ When the machine has poor rigidity.</li> </ul>

When to Increase Lead Angle
<ul style="list-style-type: none"> <li>○ Hard workpieces which produce high cutting temperature.</li> <li>○ When roughing a workpiece with large diameter.</li> <li>○ When the machine has high rigidity.</li> </ul>

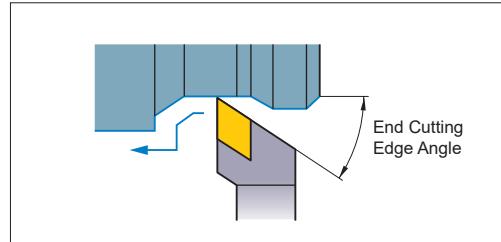


## END CUTTING EDGE ANGLE

The end cutting edge angle avoids interference between the machined surface and the tool (end cutting edge). Usually 5°–15°.

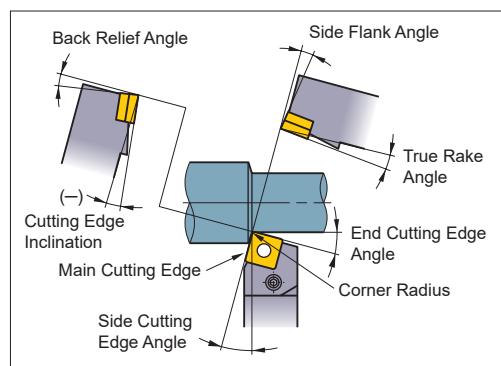
### Effects of End Cutting Edge Angle

- Decreasing the end cutting edge angle increases cutting edge strength, but it also increases cutting edge temperature.
- Decreasing the end cutting edge angle increases the back force and can result in chattering and vibration while machining.
- Small end cutting edge angle for roughing and large angle for finishing are recommended.



## CUTTING EDGE INCLINATION

Cutting edge inclination indicates inclination of the rake face. During heavy cutting, the cutting edge receives an extremely large shock at the beginning of each cut. Cutting edge inclination keeps the cutting edge from receiving this shock and prevents fracturing. 3°–5° in turning and 10°–15° in milling are recommended.

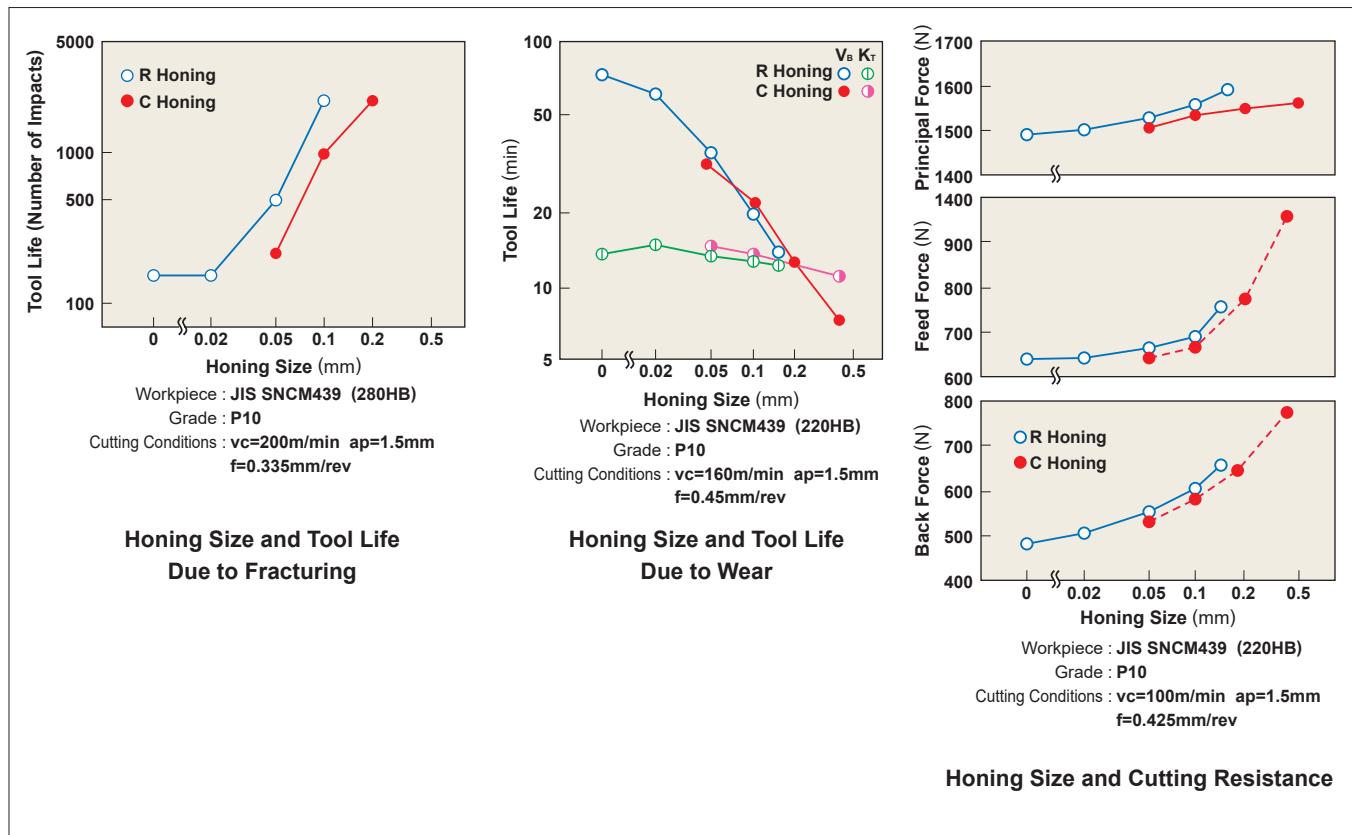
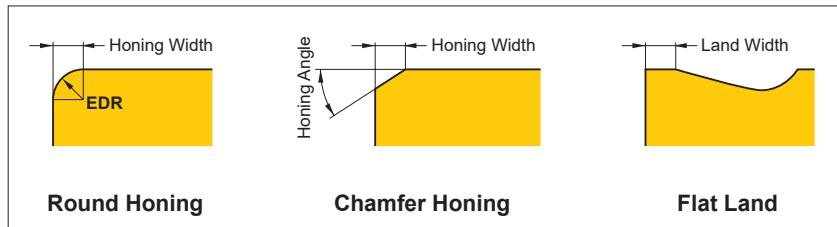


### Effects of Cutting Edge Inclination

- Negative (–) cutting edge inclination disposes chips in the workpiece direction, and positive (+) disposes chips in the opposite direction.
- Negative (–) cutting edge inclination increases cutting edge strength, but it also increases the back force of cutting resistance. Thus, chattering can easily occur.

## HONING AND LAND

Honing and land are cutting edge shapes that maintain cutting edge strength. Honing can be round or chamfer type. The optimal honing width is approximately 1/2 of the feed. Land is the narrow flat area on the rake or flank face.



## Effects of Honing

1. Enlarging the honing increases cutting edge strength, tool life and reduces fracturing.
2. Enlarging the honing increases flank wear occurrence and shortens tool life. Honing size doesn't affect rake wear.
3. Enlarging the honing increases cutting resistance and chattering.

When to Decrease Honing Size
<input type="radio"/> When finishing with small depth of cut and small feed.
<input type="radio"/> Soft workpieces.
<input type="radio"/> When the workpiece or the machine have poor rigidity.

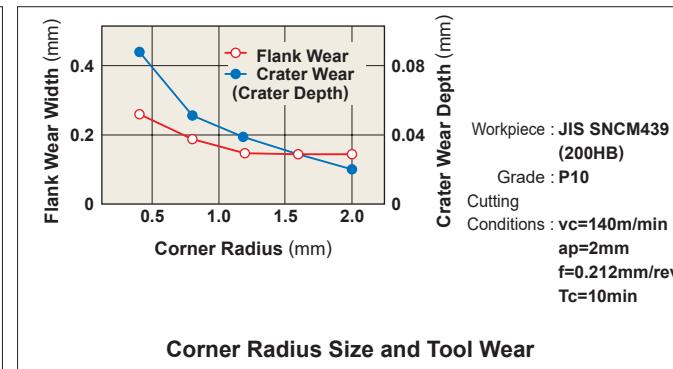
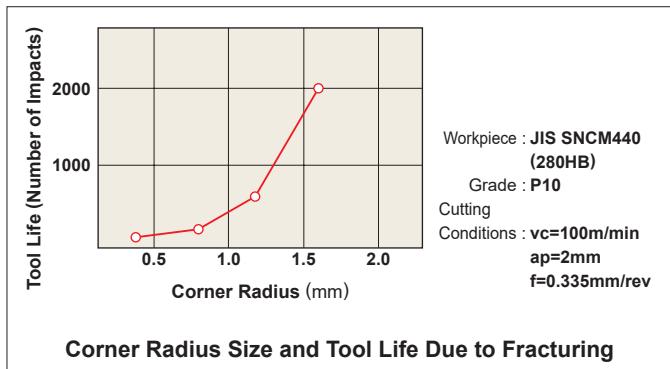
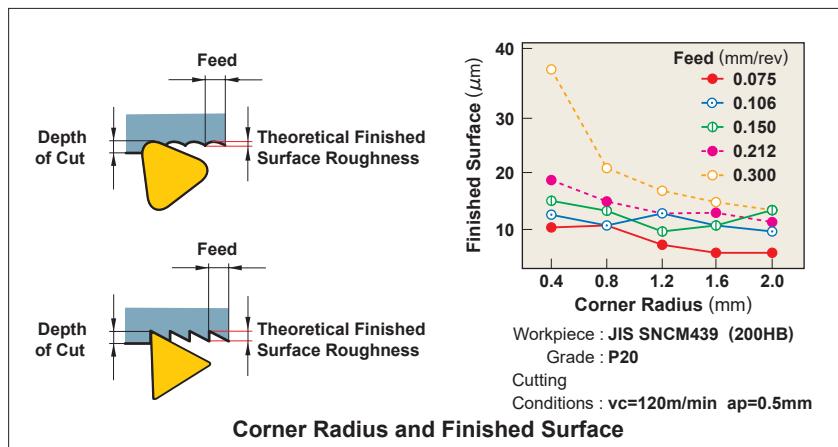
When to Increase Honing Size
<input type="radio"/> Hard workpieces.
<input type="radio"/> When the cutting edge strength is required such as for uncut surfaces and interrupted cutting.
<input type="radio"/> When the machine has high rigidity.

Note 1) Cemented carbide, coated diamond, and indexable cermet inserts have round honing as standard.

# FUNCTION OF TOOL FEATURES FOR TURNING

## RADIUS

Radius effects the cutting edge strength and finished surface. In general, a corner radius 2–3 times the feed is recommended.



## Effects of Corner Radius

- Increasing the corner radius improves the surface finish.
- Increasing the corner radius improves cutting edge strength.
- Increasing the corner radius too much increases the cutting resistance and causes chattering.
- Increasing the corner radius decreases flank and rake wear.
- Increasing the corner radius too much results in poor chip control.

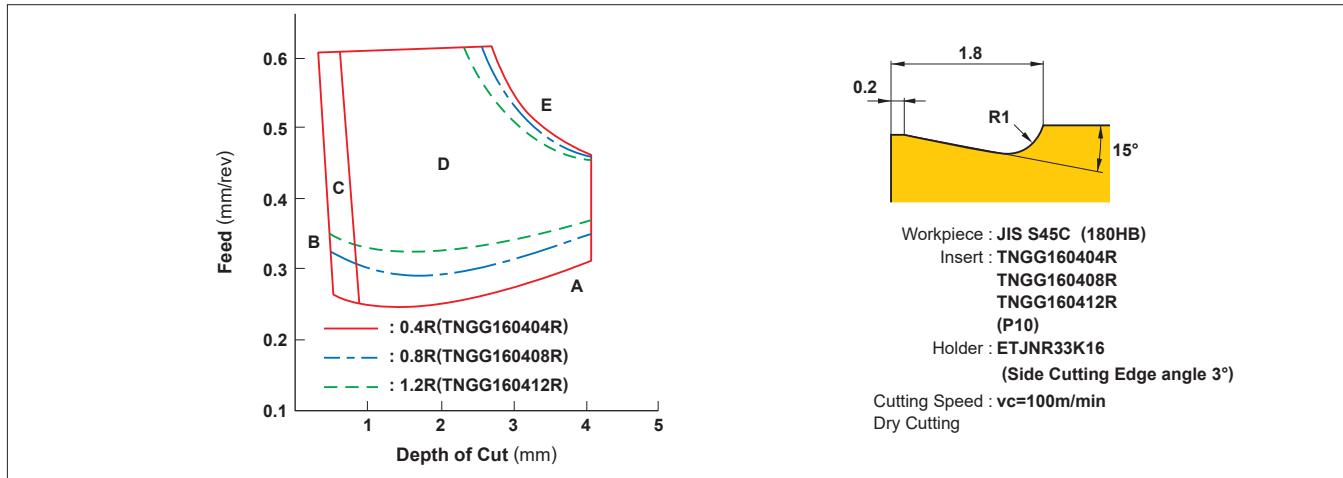
### When to Decrease Corner Radius

- Finishing with small depth of cut.
- Thin, long workpieces.
- When the machine has poor rigidity.

### When to Increase Corner Radius

- When the cutting edge strength is required such as in interrupted cutting and uncut surface cutting.
- When roughing a workpiece with large diameter.
- When the machine has high rigidity.

## Corner Radius and Chip Control Range



\*Refer to Q008 for "Shape of Chips in Steel Turning" for A, B, C, D, E in the graph above.

# FORMULAE FOR CUTTING POWER

## ■ CUTTING POWER (Pc)

$$P_c = \frac{ap \cdot f \cdot vc \cdot K_c}{60 \times 10^3 \times \eta} \text{ (kW)}$$

Pc (kW) : Actual Cutting Power  
 f (mm/rev) : Feed per Revolution  
 Kc (MPa) : Specific Cutting Force

ap (mm) : Depth of Cut  
 vc (m/min) : Cutting Speed  
 $\eta$  : (Machine Coefficient)

(Problem) What is the cutting power required for machining mild steel at cutting speed 120m/min with depth of cut 3mm and feed 0.2mm/rev (Machine coefficient 80%) ?

(Answer) Substitute the specific cutting force Kc=3100MPa into the formula.

$$P_c = \frac{3 \times 0.2 \times 120 \times 3100}{60 \times 10^3 \times 0.8} = 4.65 \text{ (kW)}$$

### ● Kc

Workpiece Material	Tensile Strength(MPa) and Hardness	Specific Cutting Force Kc (MPa)				
		0.1 (mm/rev)	0.2 (mm/rev)	0.3 (mm/rev)	0.4 (mm/rev)	0.6 (mm/rev)
Mild Steel	520	3610	3100	2720	2500	2280
Medium Steel	620	3080	2700	2570	2450	2300
Hard Steel	720	4050	3600	3250	2950	2640
Tool Steel	670	3040	2800	2630	2500	2400
Tool Steel	770	3150	2850	2620	2450	2340
Chrome Manganese Steel	770	3830	3250	2900	2650	2400
Chrome Manganese Steel	630	4510	3900	3240	2900	2630
Chrome Molybdenum Steel	730	4500	3900	3400	3150	2850
Chrome Molybdenum Steel	600	3610	3200	2880	2700	2500
Nickel Chrome Molybdenum Steel	900	3070	2650	2350	2200	1980
Nickel Chrome Molybdenum Steel	352HB	3310	2900	2580	2400	2200
Hard Cast Iron	46HRC	3190	2800	2600	2450	2270
Meehanite Cast Iron	360	2300	1930	1730	1600	1450
Grey Cast Iron	200HB	2110	1800	1600	1400	1330

## ■ CUTTING SPEED (vc)

$$vc = \frac{\pi \cdot D_m \cdot n}{1000} \text{ (m/min)}$$

vc (m/min) : Cutting Speed  
 Dm (mm) : Workpiece Diameter  
 $\pi$  (3.14) : Pi  
 n ( $\text{min}^{-1}$ ) : Main Axis Spindle Speed

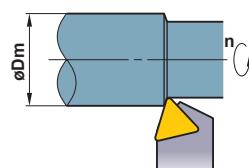
\*Divide by 1000 to change to m from mm.

(Problem) What is the cutting speed when main axis spindle speed is 700 $\text{min}^{-1}$  and external diameter is  $\phi 50$  ?

(Answer) Substitute  $\pi=3.14$ , Dm=50, n=700 into the formula.

$$vc = \frac{\pi \cdot D_m \cdot n}{1000} = \frac{3.14 \times 50 \times 700}{1000} = 110 \text{ m/min}$$

Cutting speed is 110m/min.



## ■ FEED (f)

$$f = \frac{l}{n} \text{ (mm/rev)}$$

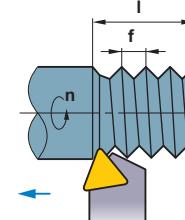
f (mm/rev) : Feed per Revolution  
 l (mm/min) : Cutting Length per Min.  
 n ( $\text{min}^{-1}$ ) : Main Axis Spindle Speed

(Problem) What is the feed per revolution when main axis spindle speed is 500 $\text{min}^{-1}$  and cutting length per minute is 120mm/min ?

(Answer) Substitute n=500, l=120 into the formula.

$$f = \frac{l}{n} = \frac{120}{500} = 0.24 \text{ mm/rev}$$

The answer is 0.24mm/rev.



## ■ CUTTING TIME (Tc)

$$T_c = \frac{l_m}{f} \text{ (min)}$$

Tc (min) : Cutting Time  
 lm (mm) : Workpiece Length  
 f (mm/min) : Cutting Length per Min.

(Problem) What is the cutting time when 100mm workpiece is machined at 1000 $\text{min}^{-1}$  with feed = 0.2mm/rev ?

(Answer) First, calculate the cutting length per min. from the feed and spindle speed.

$$l = f \times n = 0.2 \times 1000 = 200 \text{ mm/min}$$

Substitute the answer above into the formula.

$$T_c = \frac{l_m}{f} = \frac{100}{200} = 0.5 \text{ min}$$

0.5 x 60=30 (sec.) The answer is 30 sec.

## ■ THEORETICAL FINISHED SURFACE ROUGHNESS (h)

$$h = \frac{f^2}{8RE} \times 1000 (\mu\text{m})$$

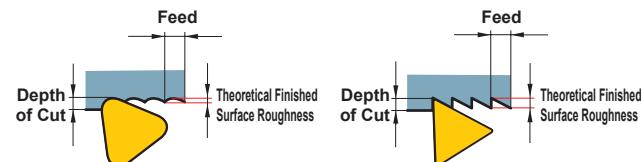
h ( $\mu\text{m}$ ) : Finished Surface Roughness  
 f (mm/rev) : Feed per Revolution  
 RE(mm) : Insert Corner Radius

(Problem) What is the theoretical finished surface roughness when the insert corner radius is 0.8mm and feed is 0.2mm/rev ?

(Answer) Substitute f=0.2mm/rev, RE=0.8 into the formula.

$$h = \frac{0.2^2}{8 \times 0.8} \times 1000 = 6.25 \mu\text{m}$$

The theoretical finished surface roughness is 6 $\mu\text{m}$ .



# TROUBLE SHOOTING FOR THREADING

Problems	Observation	Causes	Solutions
Low thread precision.	Threads do not mesh with each other.	Incorrect tool installation.	Set the insert centre height at 0mm. Check holder inclination (Lateral).
	Shallow thread.	Incorrect depth of cut. Lack of insert wear or plastic deformation resistance.	Modify the depth of cut. Refer to "Quickly generated flank wear." and "Large plastic deformation." below.
Poor surface finish.	Surface damage.	Chips wrap around or clog the work pieces.	Change to flank infeed and control the chip discharge direction. Change to an M-class insert with a 3-D chip breaker.
		The side of the insert cutting edge interferes with the workpiece.	Check the lead angle and select an appropriate shim.
	Surface tears.	Built-up edge (Welding).	Increase cutting speed. Increase coolant pressure and volume.
		Cutting resistance too high.	Decrease depth of cut per pass.
	Surface vibrations.	Cutting speed too high.	Decrease the cutting speed.
		Insufficient work piece or tool clamping.	Re-check work piece and tool clamping. (Chuck pressure, clamping allowance)
		Incorrect tool installation.	Set the insert centre height at 0mm.
Short tool life.	Flank wear quickly generated.	Cutting speed too high.	Decrease the cutting speed.
		Too many passes causes abrasive wear.	Reduce the number of passes.
		Small depth of cut for the finishing pass.	Do not re-cut at 0mm depth of cut, larger than 0.05mm depth of cut is recommended.
	Non-uniform wear of the right and left sides of the cutting edge.	The work piece lead angle and the tool lead angle do not match.	Check the work piece lead angle and select an appropriate shim.
	Chipping and fracture.	Cutting speed too low.	Increase cutting speed.
		Cutting resistance too high.	Increase the number of passes and decrease the cutting resistance per pass.
		Unstable clamping.	Check work piece deflection. Shorten tool overhang. Recheck work piece and tool clamping. (Chuck pressure, clamping allowance)
		Chip packing.	Increase coolant pressure to blow away chips. Change the tool pass to control chips. (Lengthen each pass to allow the coolant to clear the chips.) Change from standard internal cutting to back turning to prevent chip jamming.
		Non-chamfered work pieces causes high resistance at the start of each pass.	Chamfer the workpiece entry and exit faces.
	Large plastic deformation.	High cutting speed and large heat generation.	Decrease the cutting speed.
		Lack of coolant supply.	Check coolant supply is sufficient. Increase coolant pressure and volume.
		Cutting resistance too high.	Increase the number of passes and decrease the cutting resistance per pass.

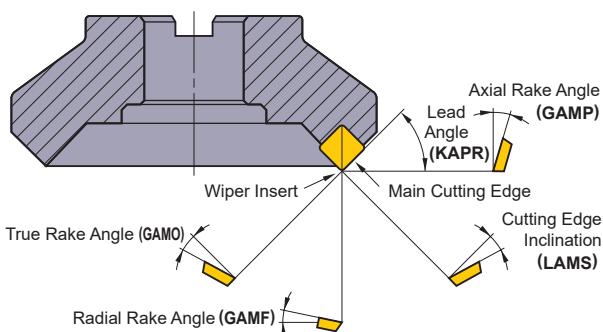


# TROUBLE SHOOTING FOR FACE MILLING

Solution		Insert Grade Selection		Cutting Conditions			Style and Design of the Tool				Machine Installation of Tool	
		Select a harder grade	Select a tougher grade	Cutting speed	Feed	Depth of cut	Engage angle	Coolant	Rake	Corner angle		
Trouble	Factors	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗	Up ↗
Deterioration of Tool Life	Insert wear quickly generated	Improper tool grade Improper cutting edge geometry Improper cutting speed	●									
	Chipping or fracturing of cutting edge	Improper tool grade Improper cutting conditions Lack of cutting edge strength. Thermal crack occurs Build-up edge occurs Lack of rigidity		●	●	●	●	●	●	●	●	●
Deterioration of Surface Finish	Poor finished surface	Improper cutting conditions Welding occurs Poor run-out accuracy Chattering	●	●	●	●	●	●	●	●	●	●
	Not parallel or irregular surface	Workpiece bending Tool clearance Large back force		●	●	●	●	●	●	●	●	●
Burr, Workpiece Chipping	Burrs, chipping	Chip thickness is too large Cutter diameter is too large Low sharpness A large corner angle		●	●	●	●		●	●	●	●
	Workpiece edge chipping	Improper cutting conditions Low sharpness A small corner angle Chattering			●	●	●		●	●	●	●
Chip Control	Poor chip dispersal, chip jamming and chip packing	Welding occurs Chip thickness is too thin Cutter diameter is too small Poor chip disposal		●	●	●		●	●	●	●	●

# FUNCTION OF TOOL FEATURES FOR FACE MILLING

## ■ FUNCTION OF EACH CUTTING EDGE ANGLE IN FACE MILLING

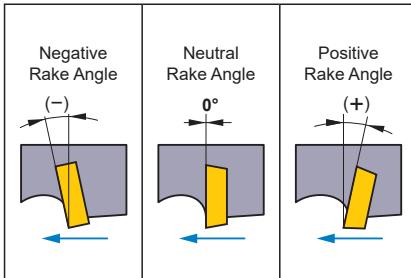


Each Cutting Edge Angle in Face Milling

Type of Angle	Symbol	Function	Effect
Axial Rake Angle	GAMP	Determines chip disposal direction.	<b>Positive :</b> Excellent machinability.
Radial Rake Angle	GAMF	Determines sharpness.	<b>Negative :</b> Excellent chip disposal.
Lead Angle	KAPR	Determines chip thickness.	<b>Small :</b> Thin chips and small cutting impact. Large back force.
True Rake Angle	GAMO	Determines actual sharpness.	<b>Positive (large) :</b> Excellent machinability. Minimal welding. <b>Negative (large) :</b> Poor machinability. Strong cutting edge.
Cutting Edge Inclination	LAMS	Determines chip disposal direction.	<b>Positive (large) :</b> Excellent chip disposal. Low cutting edge strength.

## ■ STANDARD INSERTS

### ● Positive and Negative Rake Angle

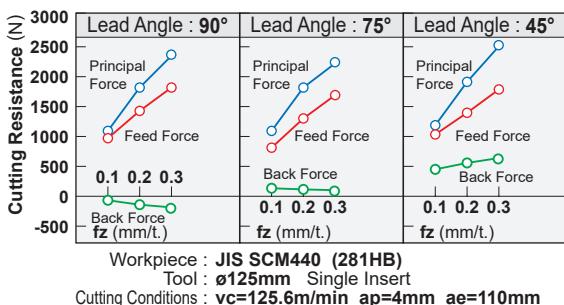


- Insert shape whose cutting edge precedes is a positive rake angle.
- Insert shape whose cutting edge follows is a negative rake angle.

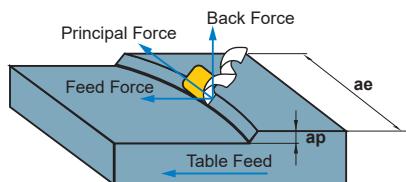
### ● Standard Cutting Edge Shape

Standard Cutting Edge Combinations	(+) Axial Rake Angle	(-) Axial Rake Angle	(+) Axial Rake Angle
	Radial Rake Angle	Radial Rake Angle	Radial Rake Angle
Double Positive (DP Edge Type)	(+)	(-)	(-)
Double Negative (DN Edge Type)	(-)	(+)	(+)
Negative/Positive (NP Edge Type)	(-)	(+)	(+)
Axial Rake Angle (GAMP)	Positive (+)	Negative (-)	Positive (+)
Radial Rake Angle (GAMF)	Positive (+)	Negative (-)	Negative (-)
Insert Used	Positive Insert (One Sided Use)	Negative Insert (Double-Sided Use)	Positive Insert (One Sided Use)
Workpiece Material	Steel	-	Steel
	Cast Iron	●	Cast Iron
	Aluminium Alloy	●	-
	Difficult-to-Cut Material	●	●

## ■ LEAD ANGLE (KAPR) AND CUTTING CHARACTERISTICS

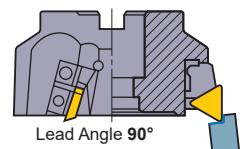


Cutting Resistance Comparison between Different Insert Shapes

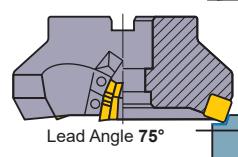


Three Cutting Resistance Forces in Milling

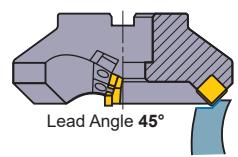
**Lead Angle 0°** Back force is in the minus direction. Lifts the workpiece when workpiece clamp rigidity is low.



**Lead Angle 15°** Lead angle 75° is recommended for face milling of workpieces with low rigidity such as thin workpieces.



**Lead Angle 45°** The largest back force. Bends thin workpieces and lowers cutting accuracy. \*Prevents workpiece edge chipping when cast iron cutting.



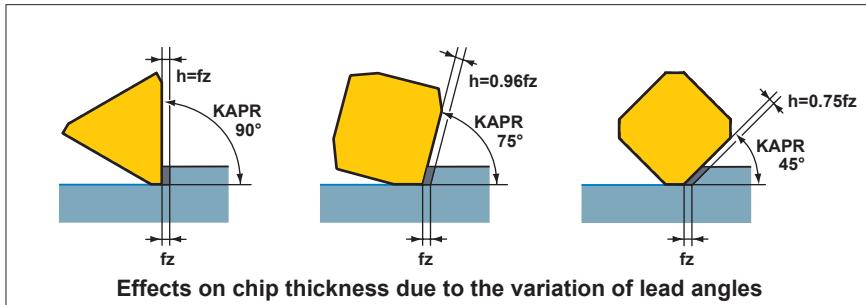
\* Principal force : Force is in the opposite direction of face milling rotation.  
\* Back force : Force that pushes in the axial direction.  
\* Feed force : Force is in the feed direction and is caused by table feed.

# FUNCTION OF TOOL FEATURES FOR FACE MILLING

## ■ APPROACH ANGLE AND THE TOOL LIFE

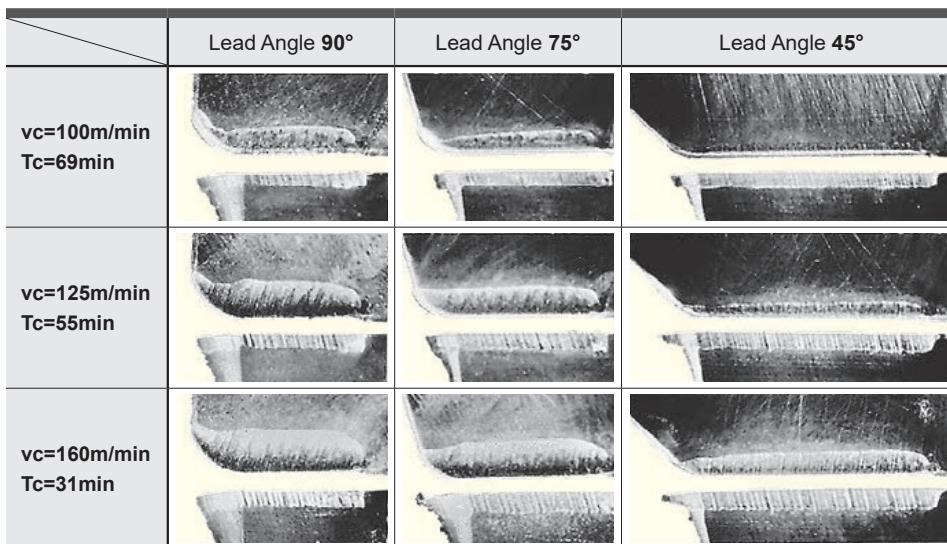
### ● Approach Angle and Chip Thickness

When the depth of cut and feed per tooth,  $f_z$ , are fixed, the smaller the lead angle (KAPR) is, then the thinner the chip thickness ( $h$ ) becomes (for a  $45^\circ$  KAPR, it is approx. 75% that of a  $90^\circ$  KAPR). This can be seen in below. Therefore as the KAPR increases, the cutting resistance decreases resulting in longer tool life. Note however, if the chip thickness is too large then the cutting resistance can increase leading to vibrations and shortened tool life.



### ● Approach Angle and Face Wear

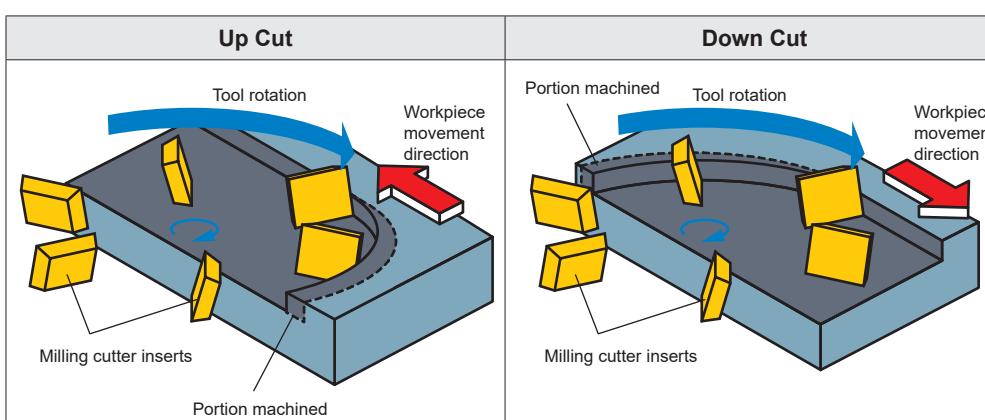
Below shows wear patterns for different lead angles. When comparing crater wear for  $90^\circ$  and  $45^\circ$  lead angles, it can be clearly seen that the crater wear for  $90^\circ$  lead angle is larger.



Workpiece : SNCM439 287HB  
Tools : DC=125mm  
Insert : M20Cemented Carbide  
Cutting Conditions : ap=3.0mm  
ae=110mm  
 $f_z=0.2mm/t$ .  
Dry Cutting

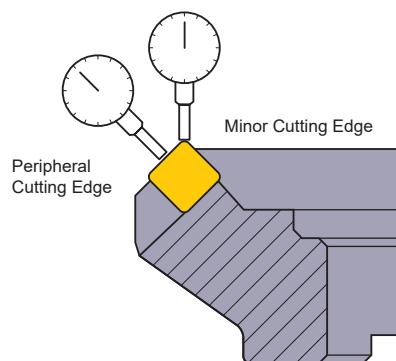
## ■ UP AND DOWN CUT (CLIMB) MILLING

When choosing a method to machine, up cutting or down cut milling (climb milling) is decided by the conditions of the machine tool, the milling cutter and the application. However, it is said that in terms of tool life, down cut (climb) milling is more advantageous.

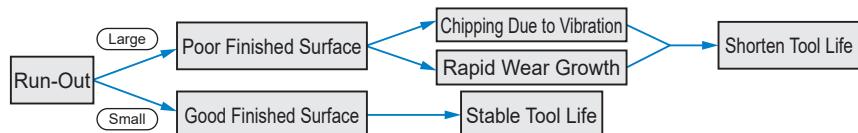


## ■ FINISHED SURFACE

### ● Cutting Edge Run-Out Accuracy

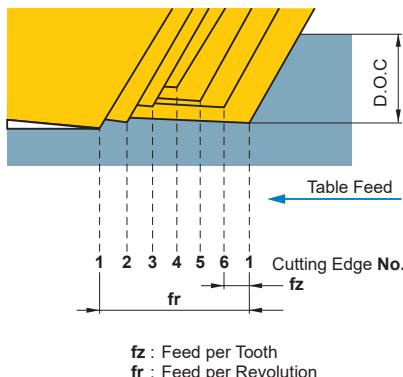


Cutting edge run-out accuracy of indexable inserts on the cutter body greatly affects the surface finish and tool life.



**Cutting Edge Run-Out and Accuracy in Face Milling**

### ● Improve Finished Surface Roughness



Since Mitsubishi Materials' normal sub cutting edge width is 1.4mm, and the sub cutting edges are set parallel to the face of a milling cutter, theoretically the finished surface accuracy should be maintained even if run-out accuracy is low.

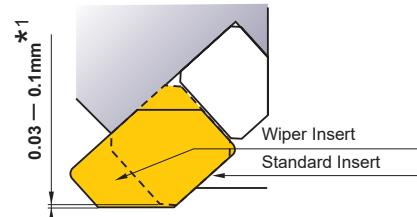
#### Actual Problems

- Cutting edge run-out.
- Sub cutting edge inclination.
- Milling cutter body accuracy.
- Spare parts accuracy.
- Welding, vibration, chattering.

#### Countermeasure

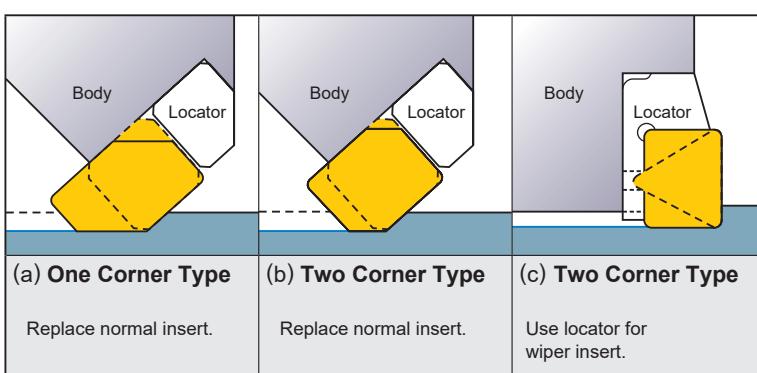
##### Wiper Insert

- \* Machine a surface that has already been per-machined in order to produce smooth finished surface.



- Replace one or two normal inserts with wiper inserts.
  - Wiper inserts be set to protrude by 0.03 – 0.1mm from the standard inserts.
- \*1. Value depends on the cutting edge and insert combination.

### ● How to Set a Wiper Insert



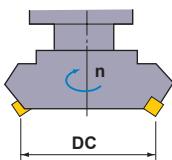
- Sub cutting edge length has to be longer than the feed per revolution.
- Too long sub cutting edge causes chattering.
- When the cutter diameter is large and feed per revolution is longer than the sub cutting edge of the wiper insert, use two or three wiper inserts.
- When using more than 1 wiper inserts, eliminate run-out of wiper inserts.
- Use a high hardness grade (high wear resistance) for wiper inserts.

# FORMULAE FOR FACE MILLING

## ■ CUTTING SPEED (vc)

$$vc = \frac{\pi \cdot DC \cdot n}{1000} \text{ (m/min)}$$

\*Divide by 1000 to change to m from mm.



vc (m/min) : Cutting Speed  
 $\pi$  (3.14) : Pi

DC(mm) : Cutter Diameter  
 $n (\text{min}^{-1})$  : Main Axis Spindle Speed

(Problem) What is the cutting speed when main axis spindle speed is 350min<sup>-1</sup> and the cutter diameter is φ125?

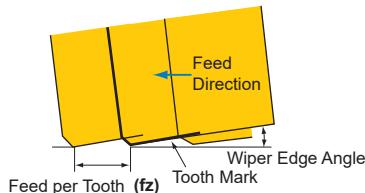
(Answer) Substitute  $\pi=3.14$ , DC=125, n=350 into the formula.

$$vc = \frac{\pi \cdot DC \cdot n}{1000} = \frac{3.14 \times 125 \times 350}{1000} = 137.4 \text{ m/min}$$

The cutting speed is 137.4m/min.

## ■ FEED PER TOOTH (fz)

$$fz = \frac{vf}{z \cdot n} \text{ (mm/t.)}$$



fz (mm/t.) : Feed per Tooth  
vf (mm/min) : Table Feed per Min.  
n (min<sup>-1</sup>) : Main Axis Spindle Speed (Feed per Revolution  $fr = z \times fz$ )

z : Insert Number

(Problem) What is the feed per tooth when the main axis spindle speed is 500min<sup>-1</sup>, number of insert is 10, and table feed is 500mm/min?

(Answer) Substitute the above figures into the formula.

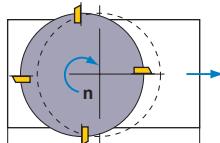
$$fz = \frac{vf}{z \cdot n} = \frac{500}{10 \times 500} = 0.1 \text{ mm/t.}$$

The answer is 0.1mm/t.

## ■ TABLE FEED (vf)

$$vf = fz \cdot z \cdot n \text{ (mm/min)}$$

vf (mm/min) : Table Feed per Min.      z : Insert Number  
fz (mm/t.) : Feed per Tooth  
n (min<sup>-1</sup>) : Main Axis Spindle Speed



(Problem) What is the table feed when feed per tooth is 0.1mm/t., number of insert is 10, and main axis spindle speed is 500min<sup>-1</sup>?

(Answer) Substitute the above figures into the formula.

$$vf = fz \cdot z \cdot n = 0.1 \times 10 \times 500 = 500 \text{ mm/min}$$

The table feed is 500mm/min.

## ■ CUTTING TIME (Tc)

$$Tc = \frac{L}{vf} \text{ (min)}$$

Tc (min) : Cutting Time  
vf (mm/min) : Table Feed per Min.  
L (mm) : Total Table Feed Length (Workpiece Length: (l)+Cutter Diameter : (DC))

(Problem) What is the cutting time required for finishing 100mm width and 300mm length surface of a cast iron (JIS FC200) block when the cutter diameter is φ200mm, the number of inserts is 16, the cutting speed is 125m/min, and feed per tooth is 0.25mm. (spindle speed is 200min<sup>-1</sup>)

Calculate table feed per min  $vf=0.25 \times 16 \times 200=800 \text{ mm/min}$

Calculate total table feed length.  $L=300+200=500 \text{ mm}$

Substitute the above answers into the formula.

$$Tc = \frac{500}{800} = 0.625 \text{ (min)}$$

0.625×60=37.5 (sec). The answer is 37.5 sec.



## ■ CUTTING POWER (Pc)

$$P_c = \frac{ap \cdot ae \cdot vf \cdot K_c}{60 \times 10^6 \times \eta}$$

**Pc (kW)** : Actual Cutting Power  
**ae (mm)** : Cutting Width  
**Kc (MPa)** : Specific Cutting Force  
**ap (mm)** : Depth of Cut  
**vf (mm/min)** : Table Feed per Min.  
 **$\eta$**  : (Machine Coefficient)

(Problem) What is the cutting power required for milling tool steel at a cutting speed of 80m/min. With depth of cut 2mm, cutting width 80mm, and table feed 280mm/min by  $\phi 250$  cutter with 12 inserts. Machine coefficient 80%.

(Answer) First, calculate the spindle speed in order to obtain feed per tooth.

$$n = \frac{1000vc}{\pi DC} = \frac{1000 \times 80}{3.14 \times 250} = 101.91 \text{ min}^{-1}$$

$$\text{Feed per Tooth } fz = \frac{vf}{z \times n} = \frac{280}{12 \times 101.9} = 0.228 \text{ mm/t.}$$

Substitute the specific cutting force into the formula.

$$P_c = \frac{2 \times 80 \times 280 \times 1800}{60 \times 10^6 \times 0.8} = 1.68 \text{ kW}$$

### ● Kc

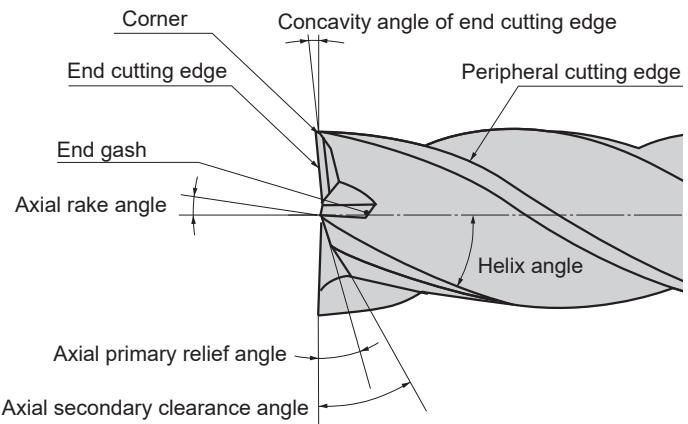
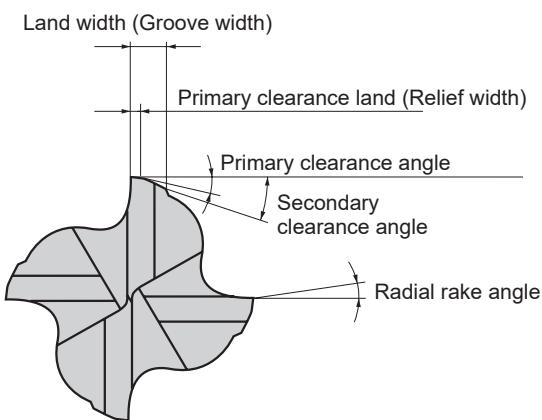
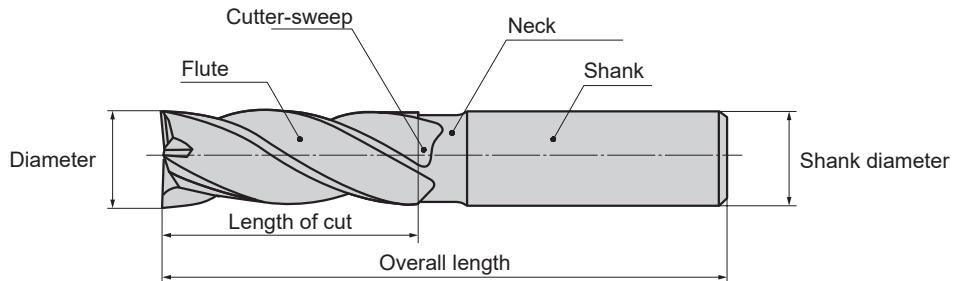
Workpiece Material	Tensile Strength (MPa) and Hardness	Specific Cutting Force Kc (MPa)				
		0.1mm/t.	0.2mm/t.	0.3mm/t.	0.4mm/t.	0.6mm/t.
Mild Steel	<b>520</b>	2200	1950	1820	1700	1580
Medium Steel	<b>620</b>	1980	1800	1730	1600	1570
Hard Steel	<b>720</b>	2520	2200	2040	1850	1740
Tool Steel	<b>670</b>	1980	1800	1730	1700	1600
Tool Steel	<b>770</b>	2030	1800	1750	1700	1580
Chrome Manganese Steel	<b>770</b>	2300	2000	1880	1750	1660
Chrome Manganese Steel	<b>630</b>	2750	2300	2060	1800	1780
Chrome Molybdenum Steel	<b>730</b>	2540	2250	2140	2000	1800
Chrome Molybdenum Steel	<b>600</b>	2180	2000	1860	1800	1670
Nickel Chrome Molybdenum Steel	<b>940</b>	2000	1800	1680	1600	1500
Nickel Chrome Molybdenum Steel	<b>352HB</b>	2100	1900	1760	1700	1530
Austenitic Stainless Steel	<b>155HB</b>	2030	1970	1900	1770	1710
Cast Iron	<b>520</b>	2800	2500	2320	2200	2040
Hard Cast Iron	<b>46HRC</b>	3000	2700	2500	2400	2200
Meehanite Cast Iron	<b>360</b>	2180	2000	1750	1600	1470
Grey Cast Iron	<b>200HB</b>	1750	1400	1240	1050	970
Brass	<b>500</b>	1150	950	800	700	630
Light Alloy (Al-Mg)	<b>160</b>	580	480	400	350	320
Light Alloy (Al-Si)	<b>200</b>	700	600	490	450	390
Light Alloy (Al-Zn-Mg-Cu)	<b>570</b>	880	840	840	810	720

# TROUBLE SHOOTING FOR END MILLING

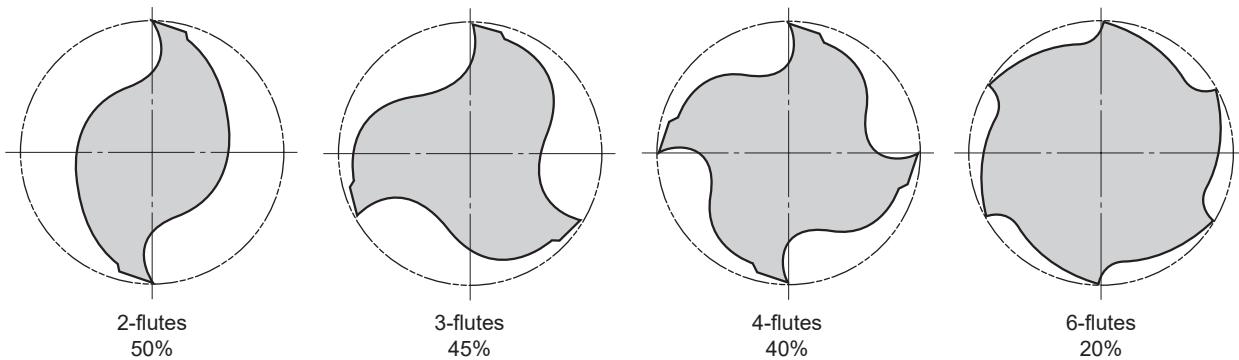
Solution		Insert Grade Selection	Cutting Conditions						Style and Design of the Tool			Machine, Installation of Tool			
			Cutting speed	Feed	Depth of cut	Pick feed	Up ↗	Down ↘	Down cut	Use air blow	Increase coolant quantity	Coolant	Up ↗ Larger	Down ↘ Smaller	Cutter rigidity
Trouble	Factors	Coated tool													
Deterioration of Tool Life	Large peripheral cutting edge wear	Uncoated end mill is used A small number of cutting edges Improper cutting conditions Up cut milling is used	●									↗			
	Severe chipping	Improper cutting conditions Fragile cutting edge Insufficient clamping force Low clamping rigidity							Down Cut		●				
	Breakage during cutting	Improper cutting conditions Low end mill rigidity Overhang longer than necessary Chip jamming					↗	↘				↗	●	●	●
Deterioration of Surface Finish	Vibration during cutting	Improper cutting conditions Low end mill rigidity Low clamping rigidity		↗	↘						↗	↗	↗	●	●
	Poor surface finish on walls	Large cutting edge wear Improper cutting conditions Chip packing.	●				↗	↘				↗	●	●	●
	Poor surface finish on faces	The end cutting edge does not have a concave angle Large pick feed					↗	↘		●	●	↗	●		
	Out of vertical	Large cutting edge wear Improper cutting conditions Lack of end mill rigidity	●				↗	↘				↗	●	●	
	Poor dimensional accuracy	Improper cutting conditions Low clamping rigidity					↗	↘				↗	●	●	●
Poor Chip Dispersal	Burr or chipping occurs	Improper cutting conditions Large helix angle					↗	↘				↗			
	Quick bur formation	Notch wear Improper cutting conditions	●				↗	↘							
	Chip packing	Metal removal too large Lack of chip pocket					↗	↘				↗	●		

# END MILL TERMINOLOGY

## ■ END MILL TERMINOLOGY



## ■ COMPARISON OF SECTIONAL SHAPE AREA OF CHIP POCKET



## ■ CHARACTERISTICS AND APPLICATIONS OF DIFFERENT-NUMBER-OF-FLUTE END MILLS

	2-flutes	3-flutes	4-flutes	6-flutes
Feature	Chip disposability is excellent. Suitable for sinking. Low cutting resistance.	Chip disposability is excellent. Suitable for sinking.	High rigidity	High rigidity. Superior cutting edge durability.
Fault	Low rigidity	Diameter is not easily measured.	Chip disposability is poor.	Chip disposability is poor.
Usage	Slotting, side milling, sinking etc. Wide range of use.	Slotting, side milling Heavy cutting, finishing	Shallow slotting, side milling Finishing	High Hardness Material Shallow slotting, side milling

# TYPES AND SHAPES OF END MILL

## ■ Peripheral Cutting Edge

Kind	Shape	Feature
Ordinary Flute		Ordinary flute type is most generally used for the slotting, side milling, and the shoulder milling, etc. Can be used for roughing, semi-finishing, and the finishing.
Tapered Flute		A tapered flute is used for milling mould drafts and angled faces.
Roughing Flute		Because a roughing tooth has a wave-like form and produces small chips. Cutting resistance is low, and is suitable for roughing. Not suitable for finishing. The tooth face is re-grindable.
Formed Flute		A corner radius cutter is shown. An infinite range of form cutters can be produced.

## ■ End Cutting Edge

Kind	Shape	Feature
Square End (Centre With Hole)		This is generally used for slotting, side milling, and shoulder milling. Sinking is not possible. Grinding is centre supported, making re-grinding accurate.
Square End (Centre Cut)		It is generally used for slotting, side milling, and shoulder milling. Vertical cutting can be performed. Re-grinding is possible.
Ball End		Suitable for profile machining and pick feed milling.
End Radius		For corner radius milling and contouring. Efficient small corner radius milling due to large diameter and small corner radius.

## ■ Shank and Neck Parts

Kind	Shape	Feature
Standard (Straight Shank)		For general use.
Long Shank		For deep slotting and has a long shank, so that adjustment of the overhang is possible.
Long Neck		For deep slotting and small diameter end mills, also suitable for boring.
Taper Neck		For best performance in deep slotting and on mould drafts.



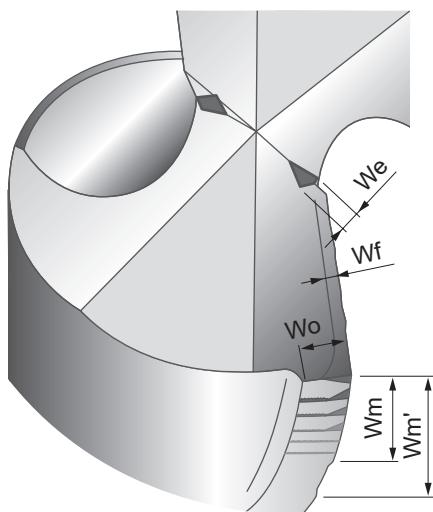
# TROUBLE SHOOTING FOR DRILLING

		Solution		Cutting Conditions						Style and Design of the Tool			Machine, Installation of Tool					
Trouble	Factors	Cutting speed	Feed	Lower feed at initial cutting	Lower feed when breaking through	Step feed	Increase accuracy of prep-hole and depth	Coolant		Chisel width	Honing width	Core thickness	Up ↗	Down ↘	Up ↗	Down ↘		
		Up ↗	Down ↘				Increase oil ratio	Increase volume	Increase coolant pressure	Shorten flute length	Decrease lip height	Use internal coolant type drill	Change to a drill with X type thinning	Increase tool installation accuracy	Shorten tool overhang	Flat workpiece face	Increase work clamping rigidity	Reduce machine backlash and increase rigidity
Deterioration of Tool Life	Drill breakage	Lack of drill rigidity Improper cutting conditions Large deflection of the tool holder Workpiece face is inclined		↙						↖ ↗	↖ ↗	↖ ↗			↖ ↗		↖ ↗	↖ ↗
	Large wear at the peripheral cutting edge and along the land	Improper cutting conditions An increase in temperature at the cutting point Poor run-out accuracy	↖ ↗					●	●				●			↖ ↗		↖ ↗
	Chipping of the peripheral cutting edge	Improper cutting conditions Large deflection of the tool holder chattering, vibration	↖ ↗		●	●									●			↖ ↗
	Chisel edge chipping	The chisel edge width is too wide Poor entry Chattering, vibration		●						↖ ↗	↖ ↗	↖ ↗					●	↖ ↗
	Hole diameter increases	Lack of drill rigidity Improper drill geometry								↖ ↗	↖ ↗	↖ ↗	●	●				
	Hole diameter becomes smaller	An increase in temperature at the cutting point Improper cutting conditions Improper drill geometry	↖ ↗				●	●					●					
	Poor straightness	Lack of drill rigidity Large deflection of the tool holder Poor guiding properties					●			↖ ↗	↖ ↗	↖ ↗	●	●	●	●	↖ ↗	↖ ↗
	Poor hole positioning accuracy, roundness and surface finish	Lack of drill rigidity Poor entry Improper cutting conditions Large deflection of the tool holder		●						↖ ↗	↖ ↗	↖ ↗		●			↖ ↗	↖ ↗
	Burrs	Burrs at the hole exit	Improper drill geometry Improper cutting conditions			●				↖ ↗	↖ ↗	↖ ↗						
Poor Chip Dispersal	Long chips	Improper cutting conditions Poor chip disposal	↖ ↗				●			↖ ↗	↖ ↗	↖ ↗	●	●				
	Chip jamming	Improper cutting conditions Poor chip disposal	↖ ↗	↖ ↗			●		●	↖ ↗	↖ ↗	↖ ↗	●	●				

# DRILL WEAR AND CUTTING EDGE DAMAGE

## ■ DRILL WEAR CONDITION

The table below shows a simple drawing depicting the wear of a drill's cutting edge. The generation and the amount of wear differ according to the workpiece materials and cutting conditions used. But generally, the peripheral wear is largest and determines a drill tool life. When regrounding, the flank wear at the point needs to be ground away completely. Therefore, if there is large wear more material needs to be ground away to renew the cutting edge.



We : Chisel edge wear width

Wf : Flank Wear (The middle of the cutting edge)

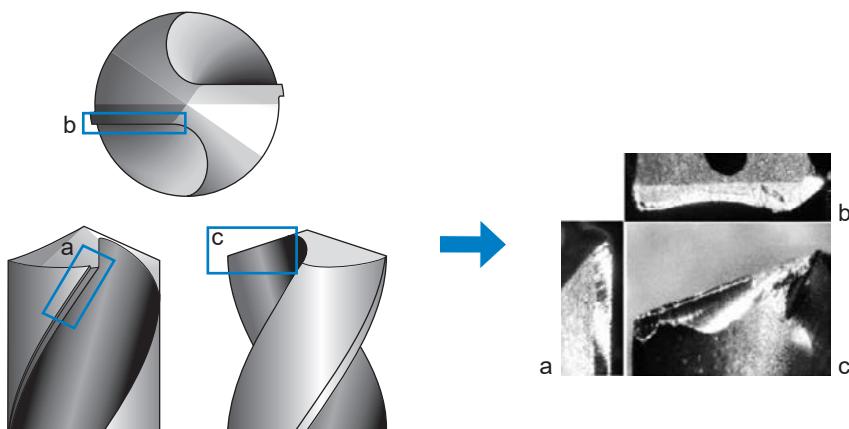
Wo : Outer corner wear width

Wm : Margin wear width

Wm' : Margin wear width (Leading edge)

## ■ CUTTING EDGE DAMAGE

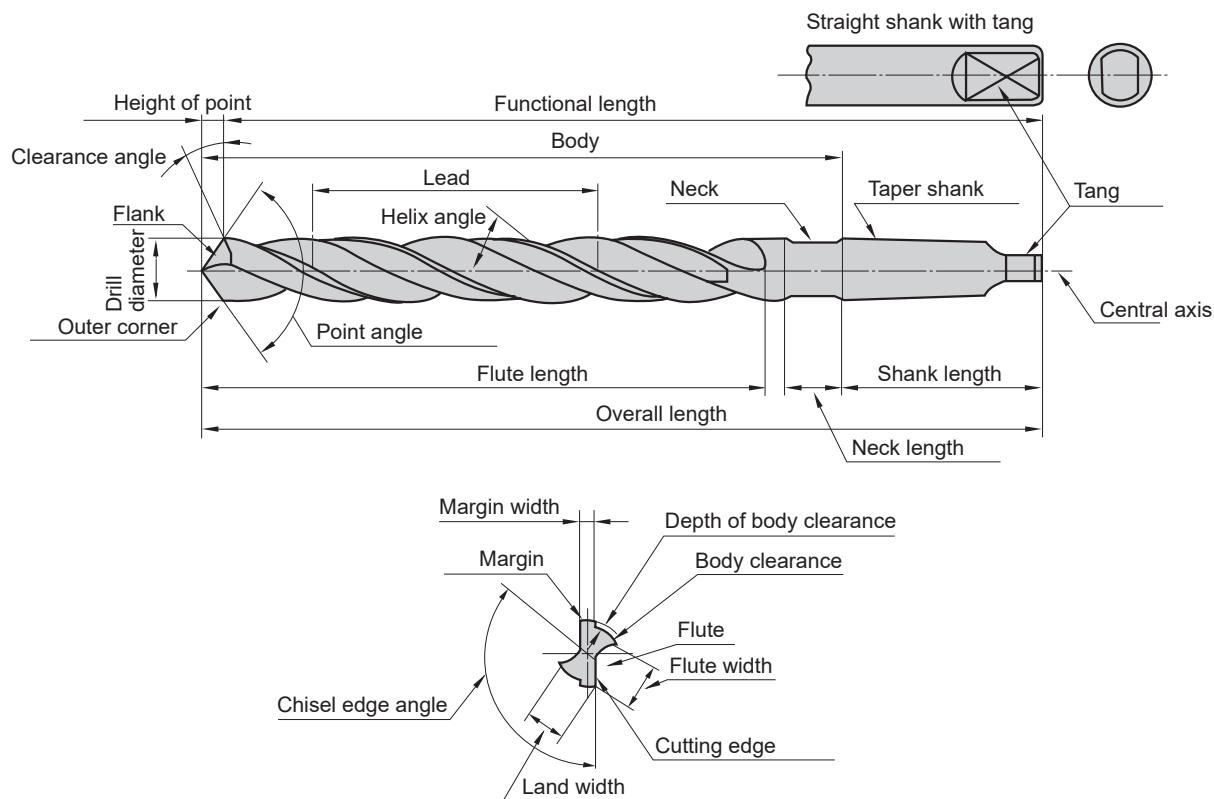
When drilling, the cutting edge of the drill can suffer from chipping, fracture and abnormal damage. In such cases, it is important to take a closer look at the damage, investigate the cause and take countermeasures.



Cutting edge damage

# DRILL TERMINOLOGY AND CUTTING CHARACTERISTICS

## ■ NAMES OF EACH PART OF A DRILL



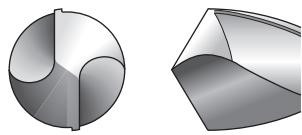
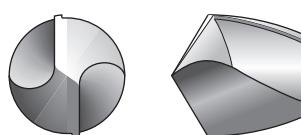
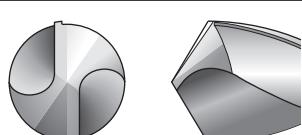
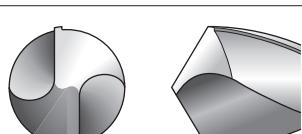
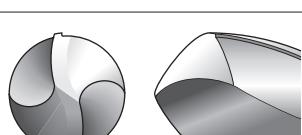
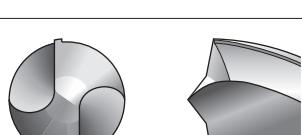
## ■ SHAPE SPECIFICATION AND CUTTING CHARACTERISTICS

Helix Angle	Is the inclination of the flute with respect to the axial direction of a drill, which corresponds to the rake angle of a bit. The rake angle of a drill differs according to the position of the cutting edge, and it decreases greatly as the circumference approaches the centre. The chisel edge has a negative rake angle, crushing the work.  High-hardness material <b>Small ◀↔ Rake angle ▶ Large Soft material (Aluminium, etc.)</b>		
Flute Length	It is determined by depth of hole, bush length, and regrinding allowance. Since the influence on the tool life is great, it is necessary to minimize it as much as possible.		
Point Angle	In general, the angle is 118° which is set differently to various applications.  Soft material with good machinability <b>Small ◀↔ Point angle ▶ Large For hard material and high efficiency machining</b>		
Web Thickness	It is an important element that determines the rigidity and chip raking performance of a drill. The web thickness is set according to applications.  Small cutting resistance Low rigidity Good chip raking performance Machinable material } <b>Thin ◀↔ Web thickness ▶ Thick</b> { Large cutting resistance High rigidity Poor chip raking performance High-hardness material, cross hole drilling, etc.		
Margin	The tip determines the drill diameter and functions as a drill guide during drilling. The margin width is determined in consideration of friction during hole drilled.  <b>Poor guiding performance Small ◀↔ Margin width ▶ Large Good guiding performance</b>		
Diameter Back Taper	To reduce friction with the inside of the drilled hole, the portion from the tip to the shank is tapered slightly. The degree is usually represented by the quantity of reduction in the diameter with respect to the flute length, which is approx. 0.04–0.1mm. It is set at a larger value for high efficiency drills and the workpiece material that allows drilled holes.		

## CUTTING EDGE GEOMETRY AND ITS INFLUENCE

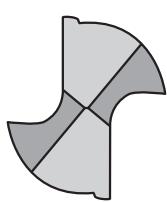
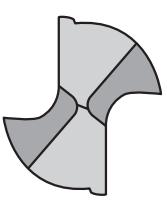
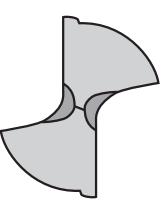
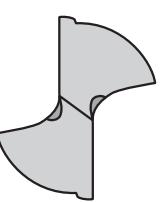
As shown in the table below, it is possible to select the most suitable cutting edge geometry for different applications. If the most suitable cutting edge geometry is selected then higher machining efficiency and higher hole accuracy can be obtained.

### Cutting Edge Shapes

Grinding Name	Shape	Features and Effect	Application
Conical		<ul style="list-style-type: none"> <li>The flank is conical and the clearance angle increases toward the centre of the drill.</li> </ul>	<ul style="list-style-type: none"> <li>General Use</li> </ul>
Flat		<ul style="list-style-type: none"> <li>The flank is flat.</li> <li>Easy grinding.</li> </ul>	<ul style="list-style-type: none"> <li>Mainly for small diameter drills.</li> </ul>
Three Flank Angles		<ul style="list-style-type: none"> <li>As there is no chisel edge, the results are high centripetal force and small hole oversize.</li> <li>Requires a special grinding machine.</li> <li>Surface grinding of three sides.</li> </ul>	<ul style="list-style-type: none"> <li>For drilling operations that require high hole accuracy and positioning accuracy.</li> </ul>
Spiral Point		<ul style="list-style-type: none"> <li>To increase the clearance angle near the centre of the drill, conical grinding combined with irregular helix.</li> <li>S type chisel edge with high centripetal force and machining accuracy.</li> </ul>	<ul style="list-style-type: none"> <li>For drilling that requires high accuracy.</li> </ul>
Radial Lip		<ul style="list-style-type: none"> <li>The cutting edge is ground radial with the aim of dispersing load.</li> <li>High machining accuracy and finished surface roughness.</li> <li>For through holes, small burrs on the base.</li> <li>Requires a special grinding machine.</li> </ul>	<ul style="list-style-type: none"> <li>Cast Iron, Aluminium Alloy</li> <li>For cast iron plates.</li> <li>Steel</li> </ul>
Centre Point Drill		<ul style="list-style-type: none"> <li>This geometry has two-stage point angle for better concentricity and a reduction in shock when exiting the workpiece.</li> </ul>	<ul style="list-style-type: none"> <li>For thin sheet drilling.</li> </ul>

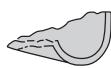
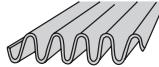
## WEB THINNING

The rake angle of the cutting edge of a drill reduces toward the centre, and it changes into a negative angle at the chisel edge. During drilling, the centre of a drill crushes the work, generating 50–70% of the cutting resistance. Web thinning is very effective for reduction in the cutting resistance of a drill, early removal of cut chips at the chisel edge, and better initial bite.

Shape	 <b>X type</b>	 <b>XR type</b>	 <b>S type</b>	 <b>N type</b>
Features	The thrust load substantially reduces, and the bite performance improves. This is effective when the web is thick.	The initial performance is slightly inferior to that of the X type, but the cutting edge is hard and the applicable range of work is wide.	Popular design, easy cutting type.	Effective when the web is comparatively thick.
Major Applications	General drilling and deep hole drilling.	Long life. General drilling and stainless steel drilling.	General drilling for steel, cast iron, and non-ferrous metal.	Deep hole drilling.

# DRILL TERMINOLOGY AND CUTTING CHARACTERISTICS

## ■ DRILLING CHIPS

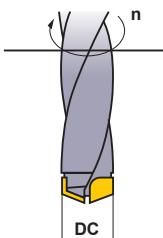
Types of Chips	Shape	Features and Ease of Raking
Conical Spiral		Fan-shaped chips cut by the cutting edge are curved by the flute. Chips of this type are produced when the feeding rate of ductile material is small. If the chip breaks after several turns, the chip raking performance is satisfactory.
Long Pitch		The generated chip comes out without coiling. It will easily coil around the drill.
Fan		This is a chip broken by the restraint caused by the drill flute and the wall of a drilled hole. It is generated when the feed rate is high.
Segment		A conical spiral chip that is broken before the chip grows into the long-pitch shape by the restraint caused by the wall of the drilled hole due to the insufficiency of ductility. Excellent chip disposal and chip discharge.
Zigzag		A chip that is buckled and folded because of the shape of flute and the characteristics of the material. It easily causes chip packing at the flute.
Needle		Chips broken by vibration or broken when brittle material is curled with a small radius. The raking performance is satisfactory, but these chips can pack closely creating.

# FORMULAE FOR DRILLING

## ■ CUTTING SPEED (vc)

$$vc = \frac{\pi \cdot DC \cdot n}{1000} \text{ (m/min)}$$

\*Divide by 1,000 to change to m from mm.



vc (m/min) : Cutting Speed  
 $\pi$  (3.14) : Pi

DC (mm) : Drill Diameter  
 $n$  ( $\text{min}^{-1}$ ) : Main Axis Spindle Speed

(Problem) What is the cutting speed when main axis spindle speed is  $1350\text{min}^{-1}$  and drill diameter is 12mm?

(Answer) Substitute  $\pi=3.14$ , DC=12,  $n=1350$  into the formula

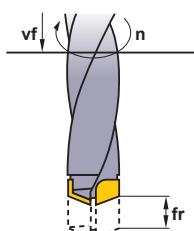
$$vc = \frac{\pi \cdot DC \cdot n}{1000} = \frac{3.14 \times 12 \times 1350}{1000} = 50.9\text{m/min}$$

The cutting speed is 50.9m/min.

## ■ FEED OF THE MAIN SPINDLE (vf)

$$vf = fr \cdot n \text{ (mm/min)}$$

vf (mm/min) : Feed Speed of the Main Spindle (Z axis)  
fr (mm/rev) : Feed per Revolution  
n ( $\text{min}^{-1}$ ) : Main Axis Spindle Speed



(Problem) What is the spindle feed (vf) when the feed per revolution is 0.2mm/rev and main axis spindle speed is  $1350\text{min}^{-1}$ ?

(Answer) Substitute  $fr=0.2$ ,  $n=1350$  into the formula

$$vf = fr \cdot n = 0.2 \times 1350 = 270\text{mm/min}$$

The spindle feed is 270mm/min.

## ■ DRILLING TIME (Tc)

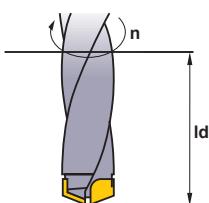
$$Tc = \frac{Id \cdot i}{n \cdot fr}$$

Tc (min) : Drilling Time  
n ( $\text{min}^{-1}$ ) : Spindle Speed  
Id (mm) : Hole Depth  
fr (mm/rev) : Feed per Revolution  
i : Number of Holes

(Problem) What is the drilling time required for drilling a 30mm length hole in alloy steel (JIS SCM440) at a cutting speed of 50m/min and a feed 0.15mm/rev?

(Answer) Spindle Speed  $n = \frac{50 \times 1000}{15 \times 3.14} = 1061.57\text{min}^{-1}$

$$Tc = \frac{30 \times 1}{1061.57 \times 0.15} = 0.188 \\ = 0.188 \times 60 \approx 11.3 \text{ sec}$$











# DIE STEELS

Classification	JIS (Others)	Aichi Steel Works	Uddeholm	Kobe Steel	Sumitomo Metal Industries	Daido Steel	Nippon Koshuha	Hitachi Metals	Mitsubishi Steel Manufacturing
Carbon Steel for Machine Structure	S50C   S55C	AUK1		KTSM2A KTSM21 KTSM22	SD10 SD17 SD21	PDS1 PXZ	KPM1		MT50C
Alloy Steel for Machine Structure	SCM440   SCM445	AUK11		KTSM3A KTSM31	SD61	PDS3			
Carbon Tool Steel	SK3	SK3				YK3	K3	YC3	
Alloy Tool Steel (For Cold Working)	SKS3	SKS3				GOA	KS3	SGT	
	SKS31					GO31	K31		
	SKS93	SK301				YK30	K3M	YCS3	
	SKD1						KD1	CRD	
	SKD11	SKD11		KAD181		DC11	KD11	SLD	
	SKD11	AUD11				DC3	KD11V	SLD2	
	SKD11		RIGOR			DC12	KDQ		
	SKD12						KD12	SCD	
		SX4							
		SX44							
		SX105V					FH5		
		TCD				DC53	KD21	SLD8	
						PD613			
						GO4		ACD37	
						GO5		HMD5	
						GO40F		HPM2T	
								YSM	
Alloy Tool Steel (For Cold Working and Others)	(P20)		IMPAK	KTSM3M		PX5	KPM30	HPM2	
	(P20)							HPM7	
	(P21)			KTSM40EF		NAK55	KAP	HPM1	
				KTSM40E		NAK80	KAP2	HPM50	
						GLD2		CENA1	
	SKD4					DH4	KD4	YDC	
	SKD5					DH5	KD5	HDC	
	SKD6					DH6	KD6		
	SKD61	SKD61	Over M Suprem			DHA1	KDA	DAC	
	SKD61						MFA		
Alloy Tool Steel (For Hot Working)	SKD62					DH62	KDB	DBC	
	SKT4					GFA	KTV	DM	
	SKD7					DH72	KDH1	YEM	
	(H10)					DH73			
	SKD8					DH41	KDF	MDC	
			QRO80M					YHD40	
						DH71			
						DH42			
						DH21			
							KDW		
							KDHM		
							AE31		
								YEM4	
	SKT4	SKT4A						YHD50	
	6F4	MPH						YHD26	
	SKT4					DH31	KDA1	DAC3	
							KDA5	DAC10	
								DAC40	
						GF78		DAC45	
						DH76		DAC55	
							TD3		
						DH2F	KDAS	FDAC	
								YHD3	
								MDC-K	
								YEM-K	

Classification	JIS (Others)	Aichi Steel Works	Uddeholm	Kobe Steel	Sumitomo Metal Industries	Daido Steel	Nippon Koshuha	Hitachi Metals	Mitsubishi Steel Manufacturing
High-Speed Tool Steel	SKH51					MH51	H51	YXM1	
	SKH55					MH55	HM35	YXM4	
	SKH57					MH57	MV10	XVC5	
						MH8	NK4	YXM60	
						MH24			
						MH7V1			
						MH64			
						VH54	HV2	XVC11	
							HM3	YXM7	
						MH85	KDMV	YXR3	
						MH88	HM9TL	YXR4	
								YXR7	
								YXR35	
Powder High-Speed Tool Steel			ASP23	KHA32		DEX20		HAP10	
			ASP30	KHA30		DEX40		HAP40	
				KHA3VN		DEX60		HAP50	
				KHA30N		DEX70		HAP63	
				KHA33N		DEX80		HAP72	
				KHA50					
				KHA77					
			ASP60	KHA60					
Stainless Steel	SUS403					GLD1			
	SUS420		STAVAX			S-STAR	KSP1	HPM38	
	SUS440C		ELMAX (Powder)	KAS440 (Powder)		SUS440C	KSP3		
	SUS420							SUS420	
	SUS630 (414)					NAK101	U630	PSL	
	Maraging Steel					MAS1C	KMS18-20	YAG	DMG300
Heat Resistant Alloy								HRNC	

# SURFACE ROUGHNESS

## SURFACE ROUGHNESS

(From JIS B 0601-1994)

Type	Code	Determination	Determination Example (Figure)
Arithmetical Mean Roughness	Ra	<p>Ra means the value obtained by the following formula and expressed in micrometer (<math>\mu\text{m}</math>) when sampling only the reference length from the roughness curve in the direction of the mean line, taking X-axis in the direction of mean line and Y-axis in the direction of longitudinal magnification of this sampled part and the roughness curve is expressed by <math>y=f(x)</math>:</p> $Ra = \frac{1}{l} \int_0^l  f(x)  dx$	
Maximum Height	Rz	<p>Rz shall be that only when the reference length is sampled from the roughness curve in the direction of the mean line, the distance between the top profile peak line and the bottom profile valley line on this sampled portion is measured in the longitudinal magnification direction of roughness curve and the obtained value is expressed in micrometer (<math>\mu\text{m}</math>).</p> <p>Note) When finding Rz, a portion without an exceptionally high peak or low valley, which may be regarded as a flaw, is selected as the sampling length.</p> $Rz = Rp + Rv$	
Ten-Point Mean Roughness	RzJIS	<p>RzJIS shall be that only when the reference length is sampled from the roughness curve in the direction of its mean line, the sum of the average value of absolute values of the heights of five highest profile peaks (Yp) and the depths of five deepest profile valleys (Yv) measured in the vertical magnification direction from the mean line of this sampled portion and this sum is expressed in micrometer (<math>\mu\text{m}</math>).</p> $Rz_{JIS} = \frac{(Y_{p1} + Y_{p2} + Y_{p3} + Y_{p4} + Y_{p5}) + (Y_{v1} + Y_{v2} + Y_{v3} + Y_{v4} + Y_{v5})}{5}$	<p> <math>Y_{p1}, Y_{p2}, Y_{p3}, Y_{p4}, Y_{p5}</math>: altitudes of the five highest profile peaks of the sampled portion corresponding to the reference length l.  <math>Y_{v1}, Y_{v2}, Y_{v3}, Y_{v4}, Y_{v5}</math>: altitudes of the five deepest profile valleys of the sampled portion corresponding to the reference length l.     </p>

## ■RELATIONSHIP BETWEEN ARITHMETICAL MEAN (Ra) AND CONVENTIONAL DESIGNATION (REFERENCE DATA)

Arithmetical Mean Roughness Ra		Max. Height Rz	Ten-Point Mean Roughness RzJIS	Sampling Length for Rz • RzJIS l (mm)	Conventional Finish Mark
Standard Series	Cutoff Value $\lambda_c$ (mm)	Standard Series			
0.012 a	0.08	0.05s	0.05z	0.08	
0.025 a	0.25	0.1 s	0.1 z	0.25	$\nabla\nabla\nabla\nabla\nabla$
0.05 a		0.2 s	0.2 z		
0.1 a	0.8	0.4 s	0.4 z	0.8	
0.2 a		0.8 s	0.8 z		
0.4 a	2.5	1.6 s	1.6 z	2.5	$\nabla\nabla\nabla$
0.8 a		3.2 s	3.2 z		
1.6 a	8	6.3 s	6.3 z	8	$\nabla\nabla$
3.2 a		12.5 s	12.5 z		
6.3 a	—	25 s	25 z	—	$\nabla$
12.5 a		50 s	50 z		
25 a	—	100 s	100 z	—	—
50 a		200 s	200 z		
100 a	—	400 s	400 z	—	—

\*The correlation among the three is shown for convenience and is not exact.

\*Ra: The evaluation length of Rz and RzJIS is the cutoff value and sampling length multiplied by 5, respectively.





## Class of Geometrical Tolerance Zone of Holes

H8	H9	H10	JS6	JS7	K6	K7	M6	M7	N6	N7	P6	P7	R7	S7	T7	U7	X7	
+14 0	+25 0	+40 0	$\pm 3$	$\pm 5$	0 -6	0 -10	-2 -8	-2 -12	-4 -10	-4 -14	-6 -12	-6 -16	-10 -20	-14 -24	-	-18 -28	-20 -30	
+18 0	+30 0	+48 0	$\pm 4$	$\pm 6$	+2 -6	+3 -9	-1 -9	0 -12	-5 -13	-4 -16	-9 -17	-8 -20	-11 -23	-15 -27	-	-19 -31	-24 -36	
+22 0	+36 0	+58 0	$\pm 4.5$	$\pm 7$	+2 -7	+5 -10	-3 -12	0 -15	-7 -16	-4 -19	-12 -21	-9 -24	-13 -28	-17 -32	-	-22 -37	-28 -43	
+27 0	+43 0	+70 0	$\pm 5.5$	$\pm 9$	+2 -9	+6 -12	-4 -15	0 -18	-9 -20	-5 -23	-15 -26	-11 -29	-16 -34	-21 -39	-	-26 -44	-33 -38 -51 -56	
+33 0	+52 0	+84 0	$\pm 6.5$	$\pm 10$	+2 -11	+6 -15	-4 -17	0 -21	-11 -24	-7 -28	-18 -31	-14 -35	-20 -41	-27 -48	-	-33 -41 -54 -67	-46 -56 -61 -77	
+39 0	+62 0	+100 0	$\pm 8$	$\pm 12$	+3 -13	+7 -18	-4 -20	0 -25	-12 -28	-8 -33	-21 -37	-17 -42	-25 -50	-34 -59	-39 -51 -64 -76	-	-	
+46 0	+74 0	+120 0	$\pm 9.5$	$\pm 15$	+4 -15	+9 -21	-5 -24	0 -30	-14 -33	-9 -39	-26 -45	-21 -51	-30 -60	-42 -72	-55 -85	-76 -106	-	
+54 0	+87 0	+140 0	$\pm 11$	$\pm 17$	+4 -18	+10 -25	-6 -28	0 -35	-16 -38	-10 -45	-30 -52	-24 -59	-38 -73	-58 -93	-78 -113	-111 -146	-	
+63 0	+100 0	+160 0	$\pm 12.5$	$\pm 20$	+4 -21	+12 -28	-8 -33	0 -40	-20 -45	-12 -52	-36 -61	-28 -68	-48 -50 -90 -53 -93	-77 -117 -147 -85 -119 -125 -159 -93 -131 -171	-107 -147 -119 -159	-	-	-
+72 0	+115 0	+185 0	$\pm 14.5$	$\pm 23$	+5 -24	+13 -33	-8 -37	0 -46	-22 -51	-14 -60	-41 -70	-33 -79	-60 -106 -151 -63 -113 -159 -109 -159 -67 -123 -113 -169	-105 -151 -113 -159 -123 -169	-	-	-	-
+81 0	+130 0	+210 0	$\pm 16$	$\pm 26$	+5 -27	+16 -36	-9 -41	0 -52	-25 -57	-14 -66	-47 -79	-36 -88	-74 -126 -126 -78 -130	-126 -88	-	-	-	-
+89 0	+140 0	+230 0	$\pm 18$	$\pm 28$	+7 -29	+17 -40	-10 -46	0 -57	-26 -62	-16 -73	-51 -87	-41 -98	-87 -144 -144 -93 -150	-	-	-	-	-
+97 0	+155 0	+250 0	$\pm 20$	$\pm 31$	+8 -32	+18 -45	-10 -50	0 -63	-27 -67	-17 -80	-55 -95	-45 -108	-103 -166 -166 -109 -172	-	-	-	-	-



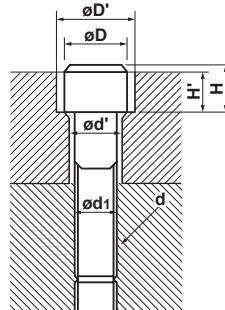
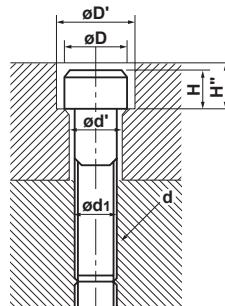


# HEXAGON SOCKET HEAD BOLT HOLE SIZE

**DIMENSIONS OF COUNTERBORING FOR  
HEXAGON SOCKET HEAD CAP SCREW AND BOLT HOLE**

Unit : mm

Nominal dimensions of thread d	M3	M4	M5	M6	M8	M10	M12	M14	M16	M18	M20	M22	M24	M27	M30
d1	3	4	5	6	8	10	12	14	16	18	20	22	24	27	30
d'	3.4	4.5	5.5	6.6	9	11	14	16	18	20	22	24	26	30	33
D	5.5	7	8.5	10	13	16	18	21	24	27	30	33	36	40	45
D'	6.5	8	9.5	11	14	17.5	20	23	26	29	32	35	39	43	48
H	3	4	5	6	8	10	12	14	16	18	20	22	24	27	30
H'	2.7	3.6	4.6	5.5	7.4	9.2	11	12.8	14.5	16.5	18.5	20.5	22.5	25	28
H''	3.3	4.4	5.4	6.5	8.6	10.8	13	15.2	17.5	19.5	21.5	23.5	25.5	29	32







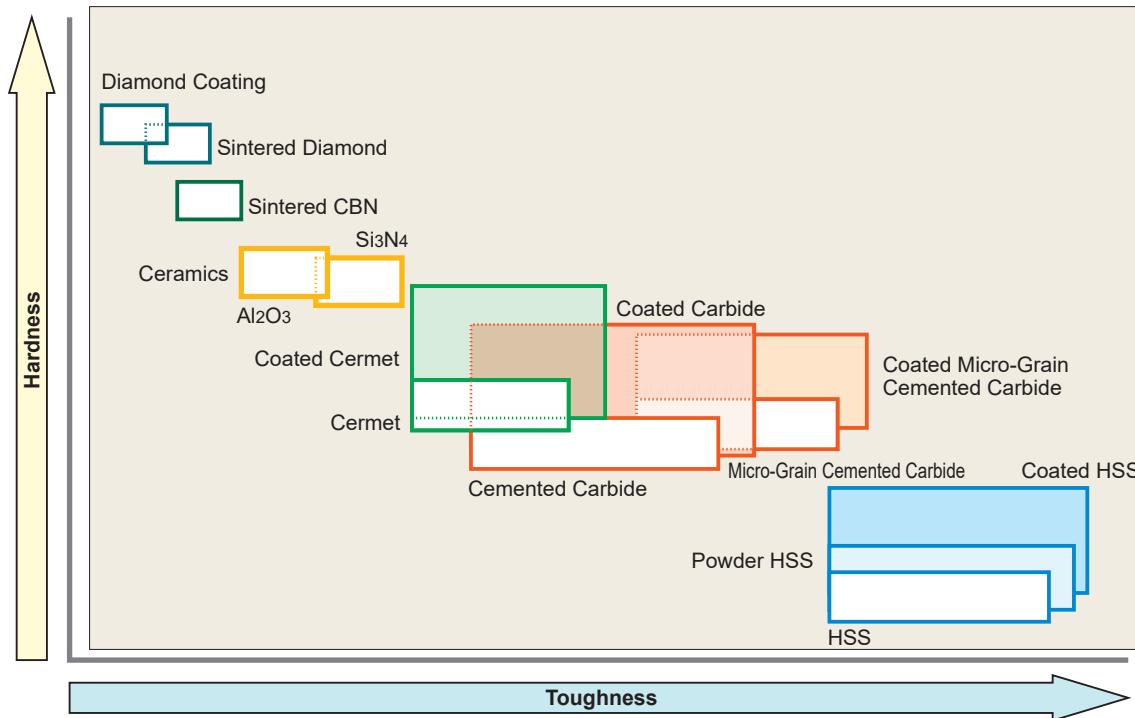
# TOOL WEAR AND DAMAGE

## CAUSES AND COUNTERMEASURES

Tool Damage Form	Cause	Countermeasure
<b>Flank Wear</b>	<ul style="list-style-type: none"> <li>• Tool grade is too soft.</li> <li>• Cutting speed is too high.</li> <li>• Flank angle is too small.</li> <li>• Feed rate is extremely low.</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high wear resistance.</li> <li>• Lower cutting speed.</li> <li>• Increase flank angle.</li> <li>• Increase feed rate.</li> </ul>
<b>Crater Wear</b>	<ul style="list-style-type: none"> <li>• Tool grade is too soft.</li> <li>• Cutting speed is too high.</li> <li>• Feed rate is too high.</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high wear resistance.</li> <li>• Lower cutting speed.</li> <li>• Lower feed rate.</li> </ul>
<b>Chipping</b>	<ul style="list-style-type: none"> <li>• Tool grade is too hard.</li> <li>• Feed rate is too high.</li> <li>• Lack of cutting edge strength.</li> <li>• Lack of shank or holder rigidity.</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high toughness.</li> <li>• Lower feed rate.</li> <li>• Increase honing. (Round honing is to be changed to chamfer honing.)</li> <li>• Use large shank size.</li> </ul>
<b>Fracture</b>	<ul style="list-style-type: none"> <li>• Tool grade is too hard.</li> <li>• Feed rate is too high.</li> <li>• Lack of cutting edge strength.</li> <li>• Lack of shank or holder rigidity.</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high toughness.</li> <li>• Lower feed rate.</li> <li>• Increase honing. (Round honing is to be changed to chamfer honing.)</li> <li>• Use large shank size.</li> </ul>
<b>Plastic Deformation</b>	<ul style="list-style-type: none"> <li>• Tool grade is too soft.</li> <li>• Cutting speed is too high.</li> <li>• Depth of cut and feed rate are too large.</li> <li>• Cutting temperature is high.</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high wear resistance.</li> <li>• Lower cutting speed.</li> <li>• Decrease depth of cut and feed rate.</li> <li>• Tool grade with high thermal conductivity.</li> </ul>
<b>Thermal Cracks</b>	<ul style="list-style-type: none"> <li>• Expansion or shrinkage due to cutting heat.</li> <li>• Tool grade is too hard. *Especially in milling.</li> </ul> 	<ul style="list-style-type: none"> <li>• Dry cutting. (For wet cutting, flood workpiece with cutting fluid)</li> <li>• Tool grade with high toughness.</li> </ul>
<b>Notching</b>	<ul style="list-style-type: none"> <li>• Hard surfaces such as uncut surfaces, chilled parts and machining hardened layer.</li> <li>• Friction caused by jagged shape chips. (Caused by small vibration)</li> </ul> 	<ul style="list-style-type: none"> <li>• Tool grade with high wear resistance.</li> <li>• Increase rake angle to improve sharpness.</li> </ul>
<b>Welding</b>	<ul style="list-style-type: none"> <li>• Cutting speed is low.</li> <li>• Poor sharpness.</li> <li>• Unsuitable grade.</li> </ul> 	<ul style="list-style-type: none"> <li>• Increase cutting speed. (For JIS S45C, cutting speed 80m/min.)</li> <li>• Increase rake angle.</li> <li>• Tool grade with low affinity. (Coated grade, cermet grade)</li> </ul>
<b>Flaking</b>	<ul style="list-style-type: none"> <li>• Cutting edge welding and adhesion.</li> <li>• Poor chip disposal.</li> </ul> 	<ul style="list-style-type: none"> <li>• Increase rake angle to improve sharpness.</li> <li>• Enlarge chip pocket.</li> </ul>
<b>Flank Wear Fracture</b> <small>* Damage for polycrystallines</small>	<ul style="list-style-type: none"> <li>• Damage due to the lack of strength of a curved cutting edge.</li> </ul> 	<ul style="list-style-type: none"> <li>• Increase honing.</li> <li>• Tool grade with high toughness.</li> </ul>
<b>Crater Wear Fracture</b> <small>* Damage for polycrystallines</small>	<ul style="list-style-type: none"> <li>• Tool grade is too soft.</li> <li>• Cutting resistance is too high and causes high cutting heat.</li> </ul> 	<ul style="list-style-type: none"> <li>• Decrease honing.</li> <li>• Tool grade with high wear resistance.</li> </ul>

# CUTTING TOOL MATERIALS

The table below shows the relationship between various tool materials, in relation with hardness on a vertical axis and toughness on a horizontal axis. Today, cemented carbide, coated carbide and TiC-TiN-based cermet are key tool materials in the market. This is because they have the best balance of hardness and toughness.

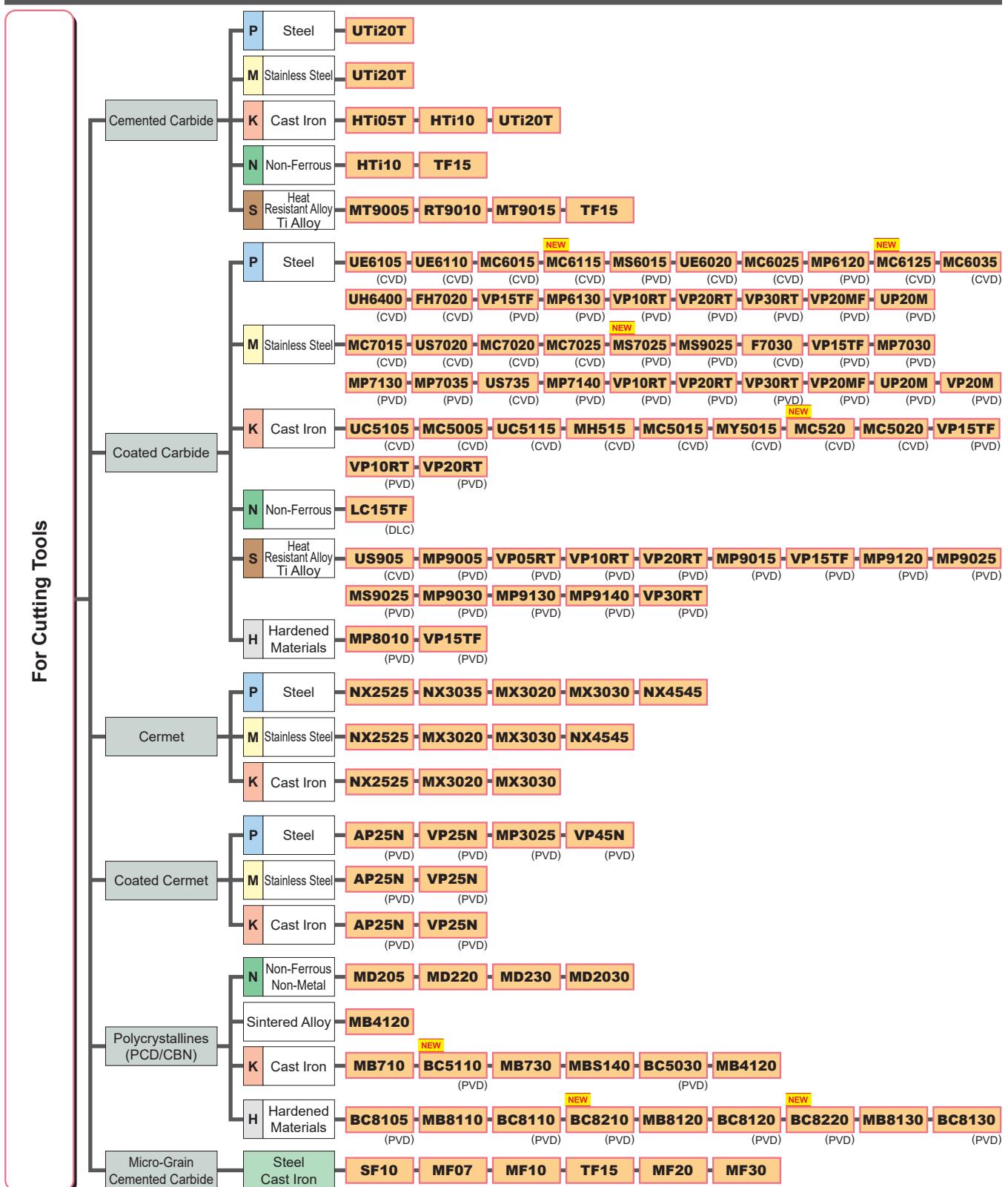


## GRADE CHARACTERISTICS

Hard Materials	Hardness (HV)	Energy Formation (kcal/g·atom)	Solubility in Iron (%.1250°C)	Thermal Conductivity (W/m·K)	Thermal Expansion ( $\times 10^{-6}/\text{K}$ )*	Tool Material
Diamond	>9000	–	Highly Soluble	2100	3.1	Sintered Diamond
CBN	>4500	–	–	1300	4.7	Sintered CBN
Si <sub>3</sub> N <sub>4</sub>	1600	–	–	100	3.4	Ceramics
Al <sub>2</sub> O <sub>3</sub>	2100	-100	÷0	29	7.8	Ceramics Cemented Carbide
TiC	3200	-35	< 0.5	21	7.4	Cermet Coated Carbide
TiN	2500	-50	–	29	9.4	Cermet Coated Carbide
TaC	1800	-40	0.5	21	6.3	Cemented Carbide
WC	2100	-10	7	121	5.2	Cemented Carbide

\*1W/m·K=2.39×10<sup>-3</sup>cal/cm·sec·°C

# GRADE CHAIN

















## 7°POSITIVE INSERT TYPE

ISO Classification	Cutting Mode	MITSUBISHI MATERIALS	Sumitomo Electric	Tungaloy	Kyocera	Dijet	MOLDINO	Sandvik	Kennametal	Seco Tools	Walter	TaeguTec
P	Finish	SMG*	FC*, SC*	JS*, 01*	CF*, CK* GQ*, GF* SKS*, SK*			UM*	LF*		FP2*	SA*
	Finish Light	FP, FV LP, SV	FB, FP, LU LB, SU	PF, PSF PS, PSS, TSF	GP, PP, VF XP		JQ	PF, UF	UF, 11 LF, FP	FF1 F1, MF2	PF4, FP4	FA, FX FG
	Light (With Wiper)	SW	LUW, SDW		WP			WF	FW	W-F1	PF	
	Medium	MV MP, Std.	GU MU	TM, 23 PM, 24	HQ, MF* XQ, GK	FT	JE	PM, UM PR, UR	MF, MP	M3 F2, M5	FP6, MP4 RP4	PC MT
	Medium (With Wiper)	MW		SW				WM	MW	W-MF2 W-M3	PM	WT
M	Finish Light	FM LM	FC*, SI* LU LB, SU	PF, PSF PS, PSS	CF*, CK* GQ*, GF* MQ*, SK*		MP	MF, UF	LF, UF FP	F1, F2 MF2	FM2* FM4	FA FG
	Medium	MM Std.	GU, MU	PM	HQ, GK			MM, UM MR, UR	MP	M3 M5	FM6 MM4, RM4	PC MT
K	Medium	MK, Std. Flat Top	MU, Flat Top*	Flat Top, CM	Flat Top*			KF, KM, UM, KR	Flat Top	F1, M3, M5	FK6, MK4 RK4, RK6	MT
N	Medium	AZ*	AG* AW*	AL*	AP* AH*	ASF*, ALU* ACB*		AL*	HP*	AL*	FN2*, PM2* MN2*	FL*
S	Finish Light	FS*, LS* FS-P*, LS-P* FJ* LS, MS	SI* GU	Std.	CE*, CK* GQ*, GF* SK*, MQ			UM* UF, MF UM, MM	LF* HP*		FM2* FM4, FM6 MM4, RM4	SA*, FA, FG PC, MT

\*Peripheral ground type insert.

Note 1) The chart above is based on data from various publications and not authorized by each individual company.

## 11°POSITIVE INSERT TYPE

ISO Classification	Cutting Mode	MITSUBISHI MATERIALS	Sumitomo Electric	Tungaloy	Kyocera	Dijet	MOLDINO	Sandvik	Kennametal	Seco Tools	Walter	TaeguTec
P	Finish Light	FV, SMG* SV	SI, FK, FB LU, LUW, LB SU, SF	01*	PP, GP, GF* SKS*, CF*, CK* PF*, XP		JQ	PF	UF, FP FW, LF		FP4	FG PC
	Medium	MV	GU, MU, US	PM TM, 23 24	HQ XQ	BM	JE	PM, UM	MF MP, MW		MP4	
M	Finish Light	SMG* SV	SU	SS* PF, PS	GF*, CK* PF*, GP, CF* SKS*		MP	MF	HP* LF		FM4	PC
	Medium	MV	GU, MU, US	PM, Std.	HQ			MM			MM4	

\*Peripheral ground type insert.

Note 1) The chart above is based on data from various publications and not authorized by each individual company.

# Memo

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